

# 2018 Formula Hybrid Electrical System Form 2 (ESF-2)

#### INTRODUCTION

The goal of the ESF is to ensure that vehicles are as safe as possible, and that they comply with the Formula-Hybrid completion rules. The ESF is divided seven main sections:

- 1 Overview
- 2 Cables, Fusing & Grounding
- 3 Isolation & Insulation
- 4 Electric Tractive System
- 5 Accumulator System
- 6 Safety Controls and Indicators
- 7 GLV System

The Cables and Fusing, and Insulation and Isolation sections are at the beginning of the ESF as these are the areas where teams most often have trouble in complying with FH rules.

A clear, concise ESF will help you to build a better car. It will also help you to pass tech testing as most common tech problems can be addressed before the car reaches the track.

# IMPORTANT INSTRUCTIONS AND REQUIREMENTS Read carefully!

- 1. Every part of this ESF must be filled with content. If a section is not relevant to your vehicle, mark it as "N/A" and describe briefly why not.
- 2. Please leave the written instructions in place and add your responses below them.
- 3. All figures and tables must be included. An ESF with incomplete tables or figures will be rejected.
- 4. The maximum length of a complete ESF is 100 pages.
- 5. Note that many fields ask for information that was submitted in your ESF-1. This information must be reentered in some cases will be different than what was entered in ESF-1, which is OK.
- 6. When completed, submit this document (in Word format *i.e. do not convert it to PDF*) to: http://formula-hybrid.com/uploads/

Please submit any questions, corrections and suggestions for improvement to: <a href="http://www.formula-hybrid.org/level2/support">http://www.formula-hybrid.org/level2/support</a>

#### **REVIEW PROCESS**

#### **NOTE: THE REVIEW PROCESS HAS CHANGED**

Feedback on your ESF occurs through both this Google Doc and the FH ticket system: <a href="http://formula-hybrid.com/level2/support/">http://formula-hybrid.com/level2/support/</a>

Your ESF will be reviewed by a team of "section reviewers" - experts in specific areas of the FH rules, AND "team reviewers" who will be your main points of contact through the competition. Reviewers will add comments coded with "//" for an informational comment, or "!!!" indicating that more information is needed, or that a concern is raised, for example:

// This diagram is well done. A suggestion in future would be to ...

!!! We have a concern regarding your accumulator construction - how did you calculate required fuse capacity?

No action is required for informational (//) comments.

(!!!) comments DO require action - either by responding to the comment in the Google doc, or opening a rules ticket (and adding a response "See FH Ticket 1234 for resolution"

When a (!!!) comment is resolved, the inspector involved may indicate this with a final comment: // RESOLVED //

If you are not receiving a response to a critical Google doc question, please open a ticket and ask for resolution.

The ESF2 is a tool for your team to make sure your car is rules compliant and ready to run at the competition. It is up to you and your team to follow up with all open items.

Our goal is to have all ESF2s reviewed in depth, and all questions resolved before the competition. This will speed up the electrical tech testing process, especially document review.

Finally, please be sure to bring supporting documentation (printed or PDF) and a READABLE full electrical schematic to the event for your physical tech inspections.

We look forward to seeing you at the track --

The Electrical Tech Team

### **TITLE PAGE**

Please include team logo, car picture, etc..





University

Name: Lafayette College

Team Name: Lafayette Motorsports

Car Number: 212

### **Main Team Contact for ESF related questions:**

Name: Waseh Ahmad

e-mail: <u>ahmadw@lafayette.edu</u>

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Must be hyperlinked!

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## **List of Abbreviations**

AIR Accumulator Isolation Relay

AMS Accumulator Management System

FH Rules Formula Hybrid Rule

GLV Grounded Low-Voltage

IMD Insulation Monitoring Device

SMD Segment Maintenance Disconnect

TS Tractive System

TSEL Tractive System Energized Light

TSMP Tractive System Measurement Point

TSV Tractive System Voltage

TSVP Tractive System Voltage Present

TSI Tractive System Interface

MARSET Master Reset

(Add more as needed)

Section 1

# **Vehicle Overview**

Person p	orimarily responsible for this section:
Name:	Waseh Ahmad
e-mail:	ahmadw@lafayette.edu
Check to	he appropriate boxes:
Vehicle	is
	<ul><li>☑ New (built on an entirely new frame)</li><li>☑ New, but built on a pre-existing frame (FSAE, FS, FH-HIP, FH electric-only, etc.)</li><li>☑ Updated from a previous year vehicle</li></ul>
Archite	cture
	☐ Hybrid
	□ Series
	□ Parallel
	☐ Hybrid in Progress (HIP¹)
	☑ Electric-only
Drive	
	☐ Front wheel
Σ	☑ Rear wheel
	☐ All-wheel
Regene	rative braking
	☐ Front wheels
Σ	☑ Rear wheels
	□ None
NARRA	TIVE OVERVIEW

 $<sup>^{\</sup>rm 1}\,{\rm HIP}$  does not need to be declared prior to the competition. If unsure, check "Hybrid"

Provide a brief, concise description of the vehicles main electrical systems including tractive system, accumulator, hybrid type (series or parallel) and method of mechanical coupling to wheels. Describe any innovative or unusual aspects of the design.

#### Include the following figures:

- **Figure 1** an electrical system block diagram showing all major parts associated with the tractive-system. (Not detailed wiring).
- Figure 2-4 Drawings or photographs showing the vehicle from the front, top, and side
- **Figure** 5– A wiring diagram superimposed on a top view of the vehicle showing the locations of all major TS components and the routing of TS wiring.
- **Figure 6-9** -- A complete TSV wiring schematic per FH Rule **EV13.2.1** showing connections between all TS components.

#### This should include:

- Accumulator Cells
- o AIRs
- o SMDs
- Fuses
- Wire Gauges
- Motor controller
- Motor
- o Pre-charge and discharge circuits
- AMD
- o IMD
- Charging port
- o Any other TS connections.

**NOTE:** Figures 6-9 is the most important diagram in the ESF

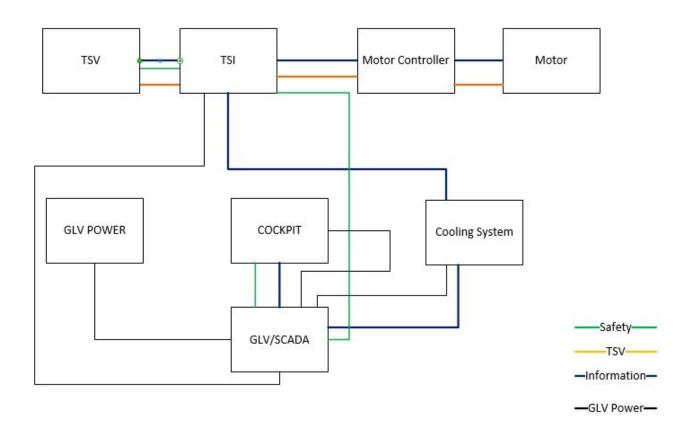


Figure 1 Electrical System Block Diagram

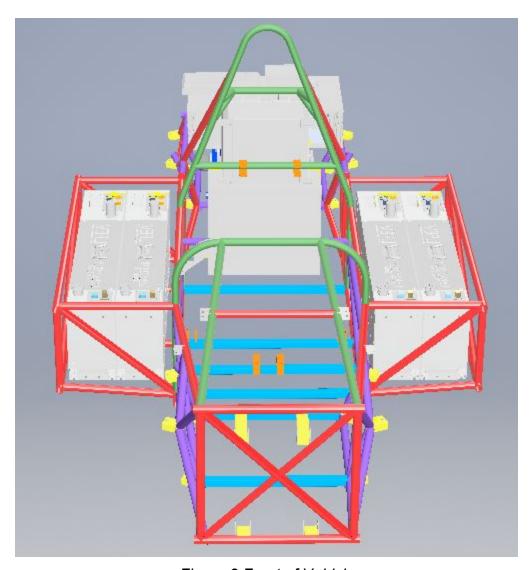


Figure 2 Front of Vehicle

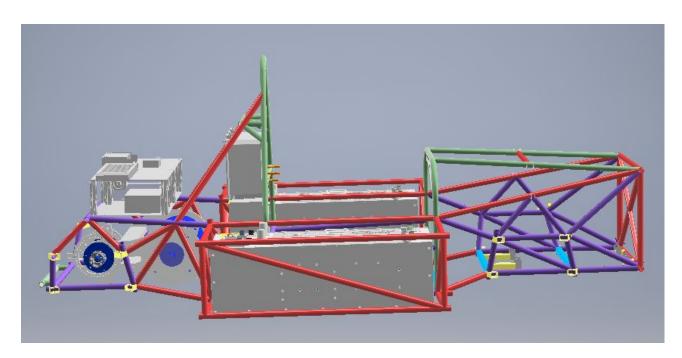


Figure 3 Side of Vehicle

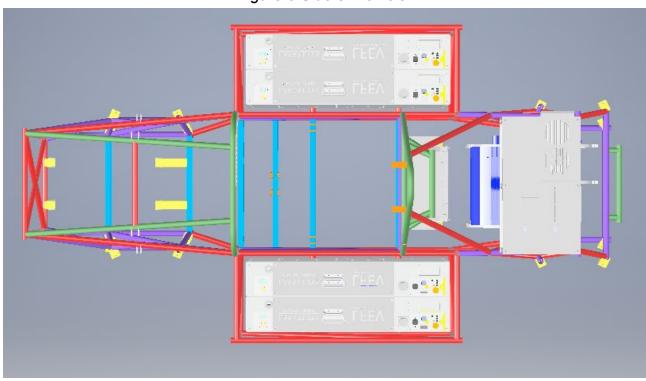


Figure 4 Top of vehicle

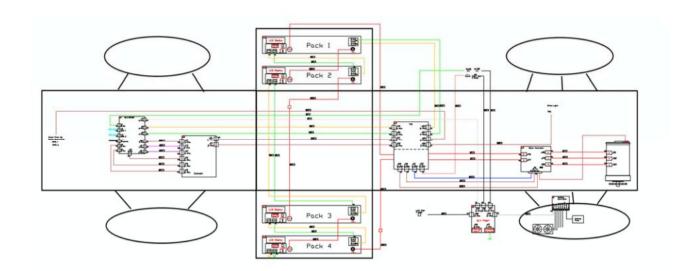


Figure 5 Location of all major TS Components

(Click for Detail)

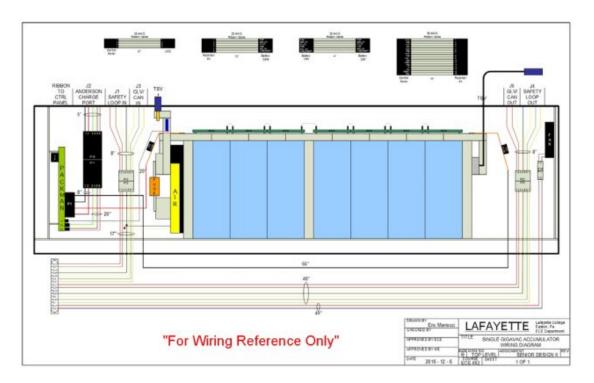


Figure 6 Packs 2-3-4 Wiring
Packs 2-3-4 Wiring (Click for detail)

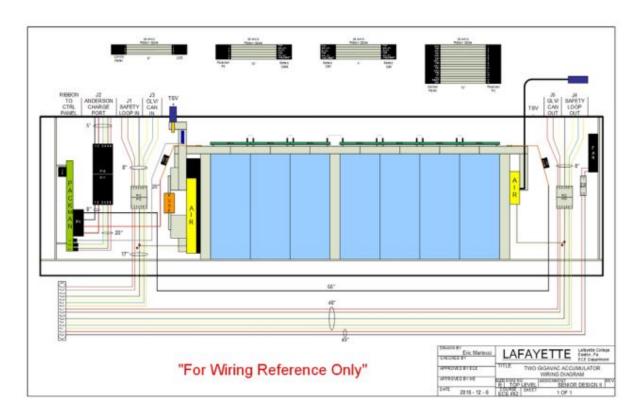


Figure 7 Pack 1 Wiring

Pack 1 Wiring (Click for Details)

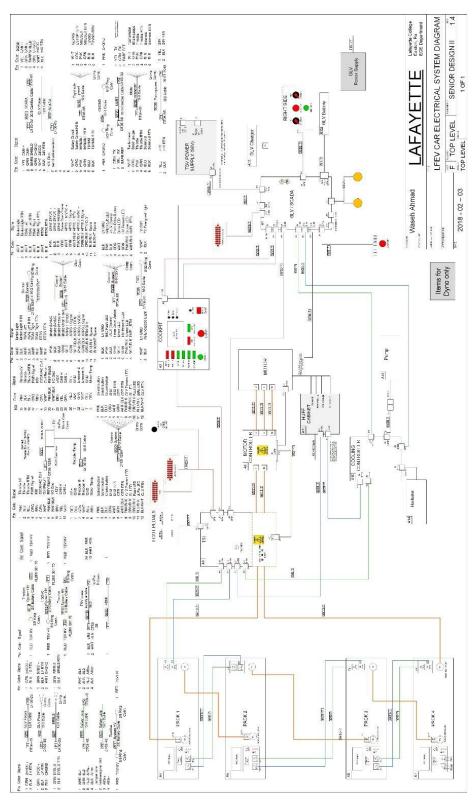
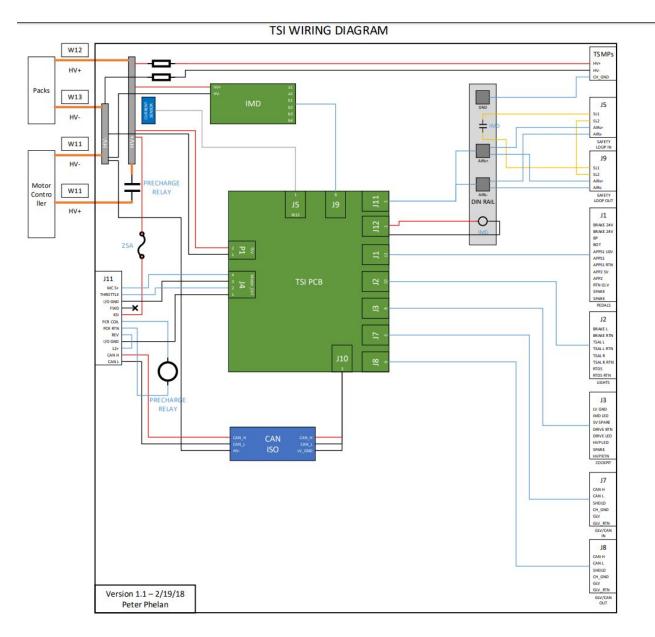


Figure 8 Wiring Diagram
Wiring Diagram (Click for details)



(Click here for more detail)

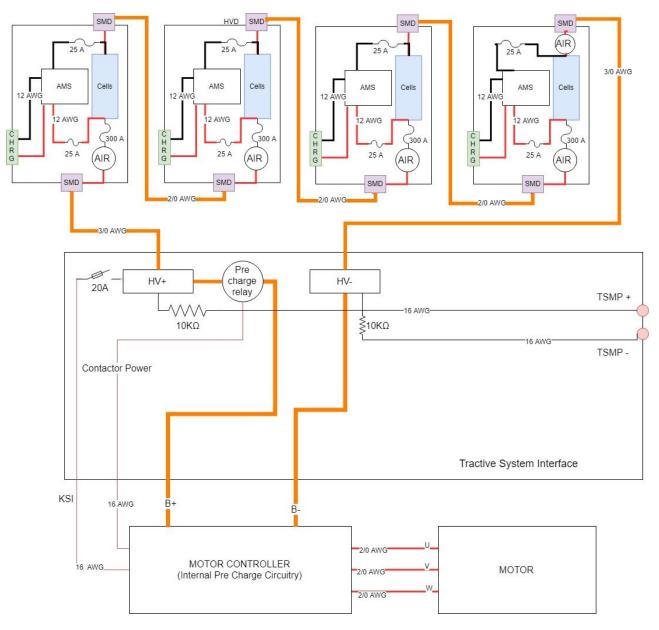


Figure 9 TSI and TSV Wiring Schematic (Click here for more detail)

#### Fill in the following table:

Item	Data
Nominal Tractive System Voltage (TSV)	89.6 VDC
Max. TSV (typically this is during charging)	96 VDC

Control System voltage (GLV)	24 VDC
Total Accumulator capacity (Wh) <sup>2</sup>	3605 Wh
Accumulator type (Lead-acid, Li-Ion, NiMH, Ultracap)	LiFePO4
Number of electric motors, total	1
Are wheel motors used?	□Yes / ⊠ No

Table 1- General Electrical System Parameters

Capacity =  $V_{nom}Ah(0.8)=3.2*28*50.3*0.8$ 

<sup>&</sup>lt;sup>2</sup> Calculate accumulator capacity per 2017 FH Rules Appendix A. Be sure to use the 2C (0.5 hour) discharge rate for the Ah value.

# Section 2

# Cables, Fusing & Grounding

Person primarily responsible for this section:

Name: Waseh Ahmad

e-mail: <u>ahmadw@lafayette.edu</u>

### 2.1 Fusing & Overcurrent Protection

List TS and GLV fuse (or circuit breaker) data, and where used

Mfg.	Fuse Part Number	Cont. Rating (A)	DC Voltage Rating	DC Interrupt Rating (A)	Where Used			
Merse n/Ferr az Shaw mut	A3T300	300 A	160V	50,000 AIC	Accumulator container; between the positive input terminal of the first cell and the AIRS.			
Littlefu se	022400 1.HXP	1 A	125V	10kA @ 125VDC	PacMAN board; separates the incoming high voltage from the accumulator from the 5V in the high voltage section of the PacMAN board.			
Littelfu se	028702 5 .PXCN	25 A	32V	1kA @ 32 VDC	Accumulator segment container; one between positive input terminal of the first cell and PacMAN board. One between the negative input terminal of the last cell and the PacMAN board.			
TE Conne ctivity	W28 -XQ1A -2	2 A	32 VDC	1kA @ 32VDC	GLV Circuit Breaker			
TE Conne ctivity	W28 -XQ1A -2	2 A	32 VDC	1kA @ 32VDC	GLV Circuit Breaker			
Littlefu se	0314.50 0HXP	0.5	125 VDC	10kA @ 125 VDC	TSI: TS to voltage monitor			
Littelfu se	031402 5.HXP	25 A	250V	400 A @ 125 VDC	Motor Controller			
Littelfu se	031402 0.HXP	20 A	250V	10kA @ 125VDC	TSI			

#### Table 2 - Fuse Table

## 2.2 Component Fusing

List major components (e.g., motor controller, dc-dc converter) and data sheet max fuse rating. Ensure that the rating of the fuse used is less than the maximum value for the component

	Fuse Part	Max Fuse	Installed Fuse Rating	
Component	Number	Rating A	А	Notes
DC-DC Converter (Murata Power Solutions, NCS6S1205C)	Internal (current fold back)	Internal	Internal	PacMAN Board
Curtis 1238 Motor Controller KSI	031402 5.HXP	400 A	25 A	
DC-DC Converter VYB20 W-Q24- S5	Internal ( short circuit, over current, and over voltage protecti on)	Internal	Internal	GLV BoB board
DC-DC Converter PDQ10-Q24-S5- D	Internal ( over voltage, input under voltage lockout, and short circuit protecti ons )	Internal	Internal	TSI Board: GLV to Iv- TSI

Isolated Module DC/DC converter RUW15SL12C	Internal (over voltage and short circuit protecti on)	Internal	Internal	TSV to TSI HV

Table 3 - Component Fuse Ratings

## 2.3 System Wire Tables

List wires and cables used in the Tractive System and the GLV system - wires protected by a fuse of 1 A or less may be omitted.

Cable capacity is the value from FH Rules Appendix E (Wire Current Capacity).

Show available fault current and how calculated.

Available fault current can be calculated from Fault Current = V source / (R source + R wiring)

Mfg.	Part Number	Size AW G	Insulation Type	Voltage Rating	Temp. Rating C	Cable Capaci ty A	Fuse Part#	Fuse Cont. A	Fuse Interrupting Rating Adc	Available Fault Current A	Where Us
IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	12K	
IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	12K	
IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	12K	
IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	12K	
IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked	600V	-70 to 150	300	A3T300	300	50 K AIC	12K	

r								т		т	т	
				elasto mer								
	IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	12K	TS
	IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	9.6K	TS
	IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	9.6K	TS
	IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	9.6K	Мо
	IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	9.6K	Мо
	IEWC	EXRA D2/0- XLEO BS	2/0	Irradia ted cross-l inked elasto mer	600V	-70 to 150	300	A3T300	300	50 K AIC	9.6K	Мо

		•							T		
WTW	WT16- 4	16	PVC	60V	-55 to 80	20	W28 -XQ1A -10	10A	1kA @ 32VDC	331	S
WTW	WT16- 4	16	PVC	60V	-55 to 80	20	W28 -XQ1A -10	10A	1kA @ 32VDC	271	S-Lo
WTW	WT16- 4	16	PVC	60V	-55 to 80	20	W28 -XQ1A -10	10A	1kA @ 32VDC	186	S-Lo
WTW	WT16- 4	16	PVC	60V	-55 to 80	20	W28 -XQ1A -10	10A	1kA @ 32VDC	165	S-Lo
WTW	WT16- 4	16	PVC	60V	-55 to 80	20	W28 -XQ1A -10	10A	1kA @ 32VDC	745	S-l
WTW	WT16- 4	16	PVC	60V	-55 to 80	20	W28 -XQ1A -10	10A	1kA @ 32VDC	1.49K	S-Loop
Prestolite Wire	15207 7	20	HDPE	60 V	-60 to	10	W28 -XQ1A -10	10A	1kA @ 32VDC	102	CA
Prestolite Wire	15207 7	20	HDPE	60 V	-60 to	10	W28 -XQ1A -10	10A	1kA @ 32VDC	84	Pad
Prestolite Wire	15207 7	20	HDPE	60 V	-60 to	10	W28 -XQ1A -10	10A	1kA @ 32VDC	62	Pad
Prestolite Wire	15207 7	20	HDPE	60 V	-60 to	10	W28 -XQ1A -10	10A	1kA @ 32VDC	55	Pad
Prestolite Wire	15207 7	20	HDPE	60 V	-60 to	10	W28 -XQ1A -10	10A	1kA @ 32VDC	181	TSI
Prestolite Wire	15207 7	20	HDPE	60 V	-60 to 125	10	W28 -XQ1A -10	10A	1kA @ 32VDC	147	TSI
L				1				1	1		1

Prestolite Wire	15207 7	20	HDPE	60 V	-60 to 125	10	W28 -XQ1A -10	10A	1kA @ 32VDC	472	GL
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	GLV Po
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	GLV Po
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	GLV/
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	G
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	2.16K	GLV I
General Cable/ Carol Brand	C2410 A.41.1 0	12	PVC	300V	-20 to 80	40	W28 -XQ1A -10	10A	1kA @ 32VDC	5K	Т
General Cable/ Carol Brand	C2405 A.46.1 0	16	PVC	300V	-20 to 90	20	W28 -XQ1A -10	10A	1kA @ 32VDC	2K	GLV/

										_	
General Cable/ Carol Brand	C2405 A.46.1 0	16	PVC	300V	-20 to 90	20	W28 -XQ1A -10	10A	1kA @ 32VDC	851	TSI
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	331	TS
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	331	Т
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	397	
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	851	GL
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	851	
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	851	٦
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	1.19K	GLV/S
Alpha Wire	5178C SL001	16	PVC	300V	-35 to 105	20	W28 -XQ1A -10	10A	1kA @ 32VDC	1.19K	GLV/S
1	1	1	i				1		i	1	

Table 4 - System Wire Table

#### 2.4 Grounding System

Describe how you keep the resistances between accessible components below the required levels as defined in FH Rules **EV8.1**. If wire is used for ground bonding, state the AWG or mm<sup>2</sup> of the wire To ensure that we will have proper grounding to the chassis, we will be using 12AWG wire for distributing the chassis ground.

Each components (TSV, TSI, Motor Controller, Cooling System, GLV/VSCADA) will have its conductive components (such as enclosure, shielded cables, conductive connectors etc.) connected to GLV ground using 12AWG cables.

#### 2.5 Conductive Panel Grounding

If carbon fiber or coated conductive panels are used in your design, describe the fabrication methods used to ensure point to point resistances that comply with **EV8.1.2**. Describe results of measurements made per **EV8.1.5**.

The GLV container is made up of fiberglass and each mechanical part within it is connected to GLV ground. As there is no concern of the fiberglass container being energized, it complies with the rules.

The TSI box is made up of Aluminum bent sheet metal with insulated paint coat on the outside. To comply with the rules, the inside of the container is connected to GLV ground. Thus post collision/accident/removal of paint, the underlying container would still be grounded.

Section 3

## **Isolation & Insulation**

Person primarily responsible for this section:

Name: Waseh Ahmad

e-mail: ahmadw@lafayette.edu

### 3.1 Separation of Tractive System and Grounded Low Voltage System

Describe how the TS and GLV systems are physically separated (**EV5.3**). Add CAD drawings or photographs of how TS and GLV are segregated in key areas of the electrical system.

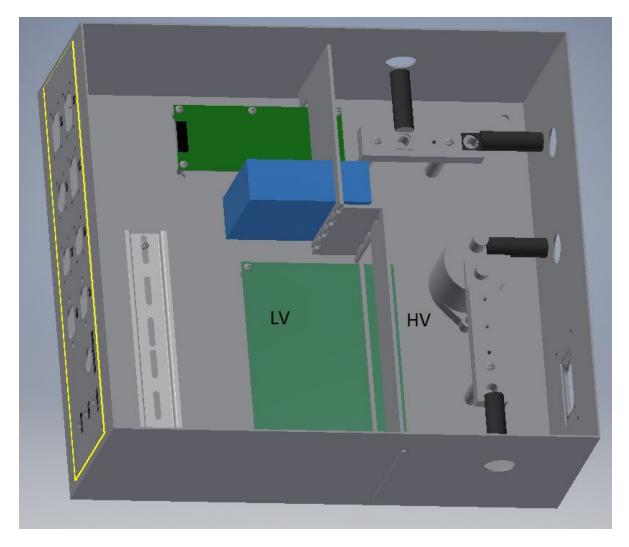


Figure 10 TSI (TS and GLV Separation)

## Figure 11 GLV Enclosure (TS GLV Separation)

The enclosures above are grounded.

List all electrical circuit boards designed by team that contain TS and GLV voltage in the following table.

Device / PCB	TS Voltage Present (V)	Minimum Spacing mm	Thru Air of Over Surface	Notes
TSI-PCB-HV-LV	Max 96	8.89 mm	OS	
TSV-PACMan	Max 24	3.80mm	OS	

Table 5 - PCB Spacings

Add a figure (board layout drawing) <u>for each</u> team-designed PCB showing that spacings comply with **EV5.5**.



Figure 12 PACMan board layout with Spacing in white

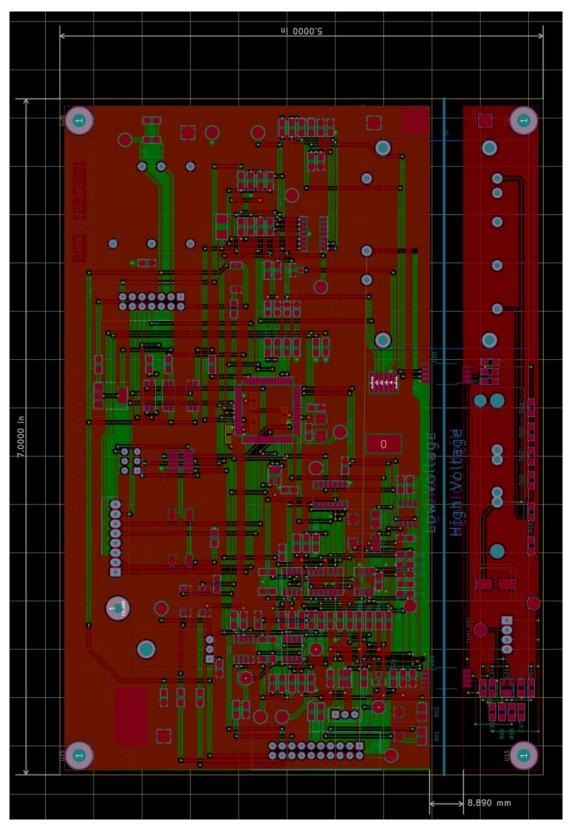


Figure 13 Team Designed PCB \_ TSI Board

List all purchased components with both TS and GLV connections (at min motor controller and AMS)

Our AMS boards are powered from the TSV system so they do not have a GLV connection. To ensure isolation there is a DC to DC converter between the cell and the AMS board.

Component	Isolation Method	Link to Document Describing Isolation	Notes			
Bender ISOMETER IR155-3203	Galvanic Isolation	http://www.bender-es.co m/fileadmin/products/doc/ IR155-32xx-V004_D0011 5_D_XXEN.pdf	Recommended by the Rules committee			
Curtis 1238 Motor Controller	Separated within TSI and then internally separated within controller	http://www.thunderstruck- ev.com/Manuals/1234_36 _38%20Manual%20Rev %20Feb%2009.pdf http://assets.curtisinstrum ents.com/Uploads/Datash eets/50265_123638E_Re vC3.pdf				
Current Sensor BBM-01	Electrical Isolation	http://www.gmw.com/mag netic_sensors/ametes/do cuments/BBM-01Spec%2 0v3.pdf	Used in Each TSV Segment and the TSI			
Can Bus Isolator CANOP	Optical Isolation	https://upverter.com/datas heet/c4e7f1a56b7f5ba03c 9a1bfb3bd7f579843b0f1d .pdf	Used in TSI			
AIRs GX14CB	Electrical Isolation	http://www.gigavac.com/si tes/default/files/catalog/sp ec_sheet/gx14.pdf	Total of 5 AIRs, one in each Segment and an extra one in Pack 4			

## 3.2 Isolation & Insulation

Provide a list of containers that have TS and GLV wiring in them. If a barrier is used rather than spacing, identify barrier material used (reference Table 7- Insulating Materials).

Container Name	Segregation by Spacing (Y or N)	How is Spacing maintained	Actual Measured Spacing mm	Alt – Barrier Material P/N	Notes
TSI	Y	Physical barrier	15	Garolite/ Acrylic	N/A
Motor	Y	Physical	N/A	Garolite/	N/A
Controller		barrier		Acrylic	
Pack 1	Y	Physical barrier	10	Garolite	N/A
Pack 2	Y	Physical barrier	10	Garolite	N/A
Pack 3	Y	Physical barrier	10	Garolite	N/A
Pack 4	Y	Physical barrier	10	Garolite	N/A

Table 6 – List of Containers with TS and GLV wiring

List all insulating barrier materials used to meet the requirements of EV2.4 or EV5.4

Insulating Material / Part Number	UL Recognize d(Y / N)	Rated Temperatur e °C	Thickness mm	Notes
Garolite	Υ	93.8 - 148.8	17.145	N/A

#### Table 7- Insulating Materials

#### 3.3 Conduit

List different types of conduit used in the design. Specify location and if manufacturer's standard fittings are used. Note Virtual Accumulator Housing FH Rules **EV2.12** requires METALLIC type LFMC.

#### NO conduit is being used

Describe how the conduit is anchored if standard fittings are not used.

Conduit Type	MFR	Part Number	Diameter Inch or mm	Standard Fittings (Y or N)	Location / Use

Table 8 - Conduit Data

Is all conduit contained within the vehicle Surface Envelope per **EV3.1.6**? (**Y or N**). Does all conduit comply with **EV3.2**? (**Y or N**).

#### 3.4 Shielded dual-insulated cable

If Shielded, dual-insulated cable per EV3.2.5 used in the vehicle, provide specifications and where used:

MFR	Part Number	Cross Section mm2	Shield grounded at both ends (Y or N)	Location / Use
IEWC	EXRA D2/0-X LEOBS	70	Y	Between TSV containers; TSV to TSI;TSI to motor controller; Motor Controller to Motor

Table 9 - Shielded Dual Insulated Cable Data

## 3.5 Firewall(s)

#### **Description/materials**

Describe the concept, layer structure and the materials used for the firewalls. Describe how all firewall requirements in FH Rules **T4.5** are satisfied. Show how the low resistance connection to chassis ground is achieved.

The firewall is made out of Al sheet, steel welded to frame, and covered with fire resistant tape. Layers: Sheet aluminum (1.5 mm aluminum), fire resistant tape

The Al sheets run underneath the driver and behind the main roll hoop to separate the driver from the fuel tanks, all components of fuel supply, cooling systems, GLV, TSI, external engine oil systems, and all conductors carrying tractive system voltages. The panels are mechanically fastened in place and sealed at the joints. The firewall is extended upward behind the driver to a height where a straight line cannot be drawn between 150 mm below the top of the tallest driver's helmet and the T4.5.1 components behind the driver. The batteries are contained within an Al casing of 1/8" and thus act as the side accumulator firewalls as checked with the FSAE rules committee.

The Chassis is connected to GLV ground using a 12 AWG cable.

#### Position in car

Provide CAD-rendering or photographs showing the location of the firewall(s).

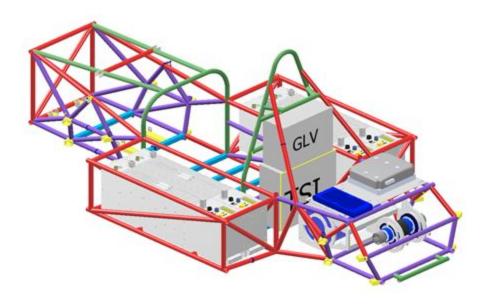


Figure 14 Battery Pack Firewall Containers Relative to Driver Seat

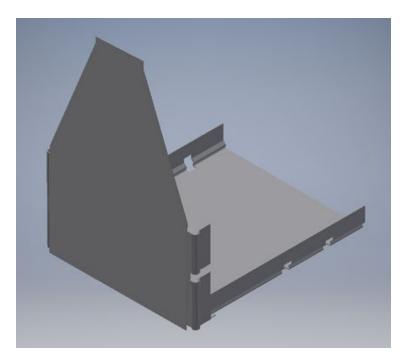


Figure 15 Driver Seat Firewall CAD drawing
Section 4

# **Electric Tractive System**

Person primarily responsible for this section:

Name:	Waseh Ahmad
e-mail:	ahmadw@lafayette.edu

# 4.1 Motor(s)

Describe the motor(s) used and reason for this particular choice. Add additional tables if multiple motor types are used

We are using this motor as it is the appropriate motor recommended by the manufacturer, to be used with the specifically chosen Motor Controller. Its nominal voltage and current usage are within range of the designed batteries.

Manufacturer and Model:	HPEVS AC 50-27.28.11	
Motor type (PM, Induction, DC Brush)	Induction	
Number of motors of this type used	1	
Nominal motor voltage (Vrms I-I or Vdc)	96	
Nominal / Peak motor current (A or A/phase)	Nom: 200A / Peak: 650A	
Nominal / Peak motor power	Nom: 19 HP / Peak: 71 HP	
Motor wiring – conductor size and type	3/8" Ring Connectors w/ 00 Gauge Copper Wire	

Table 10 - Motor Data

Provide calculations for currents and voltages. State how this relates to the choice of cables and connectors used.

Cable used is the 2/0 Gauge cable which has a capacity of 300A. For peak current protection, 300A fuses are used within the TSV packs.

#### 4.2 Motor Controller

Describe the motor controller(s) used and reason for this particular choice. Add additional tables if multiple motor controller types are used.

We are using the Curtis 1238 due to its voltage rating allowing for 96V input as well as its nominal current rating.

Manufacturer and Model:	Curtis 1238
Number of controllers of this type used:	1
Maximum Input voltage:	130 V
Nominal Input Current (A)	200 A
Max Input Fuse (A) per Mfr.	650 A
Output voltage (Vac I-I or Vdc)	96 V <sub>AC</sub>
Isolation voltage rating between GLV (power supply or control inputs) and TS connections	1 KVDC
Is the accelerator galvanically isolated from the Tractive System per <b>EV3.5 &amp; EV5</b> ?	⊠Yes / □ No

Table 11 - Motor Controller Data

If the answer to the last question is NO, how do you intend to comply with **EV3.5** (an external isolator is acceptable).

Provide calculations for currents and voltages. State how this relates to the choice of cables and connectors used.

The values for voltages/currents are provided in the table above. The choice of cable is 2/0 AWG cables as the current rating is above that of the nominal input current to the controller. Connectors used are 3/8 Ring terminals, appropriate for the 2/0 Cable used.

# 4.3 Tractive System Measurement Points (TSMP)

The TSMP must comply with FH Rule **EV10.3**. Describe the TSMP housing and location. Describe TSMP electrical connection point.

TSMP Output Protection Resistor Value	10 kΩ
---------------------------------------	-------

Resistor Voltage Rating	460 V
Resistor Power Rating	5 W

Table 12 – TSMP Resistor Data

The TSMP are located on the TSI box enclosure along with the GLV ground. They are Shrouded 4 mm banana jacks that accept shrouded (sheathed) banana plugs with nonretractable shrouds. The TSMP connect to the TSV positive and negative terminals incoming to the TSI enclosure.

#### 4.4 Pre-Charge circuitry

Describe your design for the pre-charge circuitry. Describe wiring, connectors and cables used.

- Include a schematic of the pre-charge circuit
- Include a plot of calculated TS Voltage vs. time
- Include a plot of calculated Current vs. time
- Include a plot of resistor power vs time.

As per Curtis 1238 data, the pre-charge circuit is built into the motor controller. <a href="http://www.evwest.com/catalog/product\_info.php?products\_id=103">http://www.evwest.com/catalog/product\_info.php?products\_id=103</a>

As per page 103 of the manual,

http://www.thunderstruck-ev.com/Manuals/1234\_36\_38%20Manual%20Rev%20Feb%2009.pdf , the capacitor bank charges to 3V of the KSI i.e. Battery voltage. This is well within 90% of the nominal or max voltage for the TSV. As it also allowed to pre-charge the circuit for a conservative time as well, the motor-controller pre-charge also may charge the capacitor bank for one second.

If the shutdown sequence is initiated, no power will be supplied from the TSV to TSI to motor controller and the pre-charge circuit will shut down and not charge.

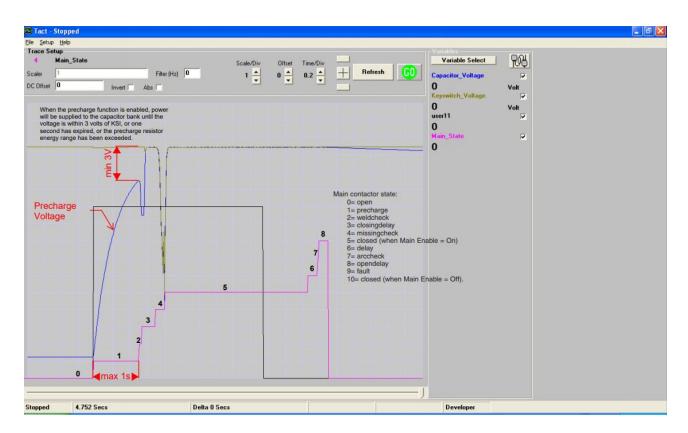


Figure 16 Motor Controller Startup -Pre-Charge

# Provide the following information:

Resistor Type:	N/A Within Motor Controller
Resistance:	Ω
Continuous power rating:	W
Overload power rating:	W for sec
Voltage rating:	V

Table 13 - Data for the pre-charge resistor

Relay MFR & Type:	GIGAVAC GV200QA
Contact arrangement (e.g. SPDT)	SPST- Normally open
Continuous DC contact current (A):	400 A
Contact voltage rating (Vdc).	1000 V

Table 14 - Data of the pre-charge relay

# 4.5 Discharge circuitry

Describe your concept for the discharge circuitry. Describe wiring, connectors and cables used.

- Include a schematic of the pre-charge circuit
- Include a plot of calculated TS Voltage vs. time
- Include a plot of calculated "Discharge current" vs. time
- Include a plot of resistor power vs time.

# The motor controller does have internal capacitance but has its own discharge circuit designed by Curtis.

There is a capacitor across the HV in the TSI as shown in the figure below. The capacitor used is 10uF with a connected resistance of 254.3K for a time constant of

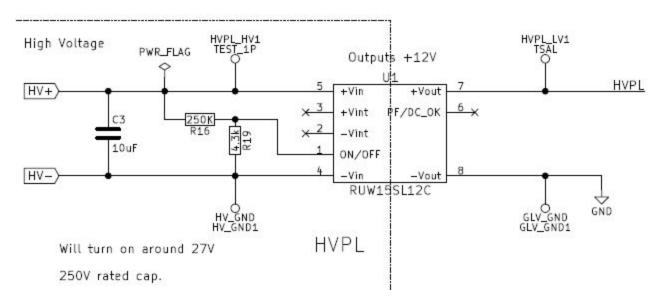


Figure 17 Discharge Circuit for Capacitor in TSI

#### Provide the following information:

Resistor Type:	ERA-6AEB432V Series ERJ-6ENF2493V
Resistance:	254.3kΩ
Continuous power rating:	0.125 W
Overload power rating:	1 W for 5 sec

Voltage rating:	200 V
Maximum expected current:	0.378 mA
Average current:	0.352 mA

Table 15 - Data of the discharge circuit.

Max Current = 96/(254.3 kohm)

Average Current = 89.6/(254.3 kohm)

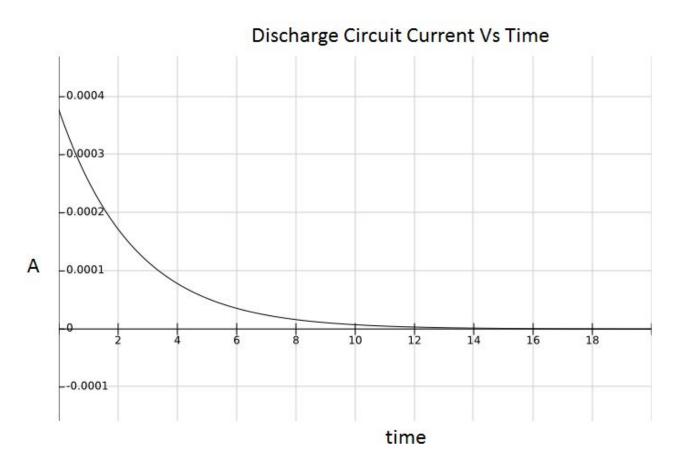


Figure 18 Calculated Discharge Current Vs Time

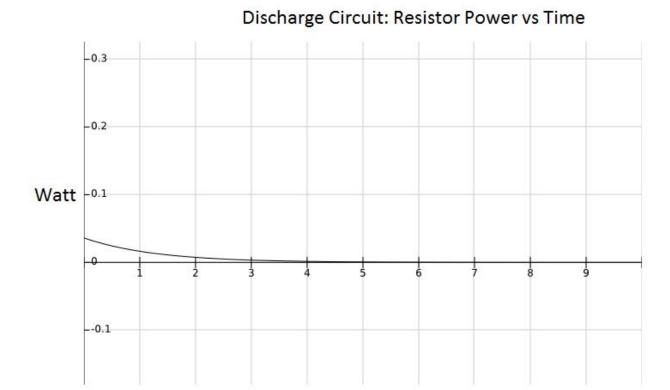


Figure 19 Discharge Circuit Resistor Power vs Time

time

## 4.6 HV Disconnect (HVD)

Describe your design for the HVD and how it is operated, wiring, and location. Describe how your design meets all requirements for **EV2.9**.

The HVD is an Amphenol PowerLok connector, connected to pack 2, coming from pack 3. It is operated by manually unplugging the connector from its receptacle. It can maintain its disconnected state as long as it is not connected to the receptacle, fitted using the keying method for the connector. It is accessible by the driver and can be removed within 10 seconds of ready to race conditions. It is also located near the middle of the series of cells. As such, if disconnected, it will de-energize the TSAL and the TSMPs.

#### 4.7 Accelerator Actuator / Throttle Position Sensor

Describe the accelerator actuator and throttle position sensor(s) used, describe additional circuitry used to check or condition the signal going to the motor controller. Describe wiring, cables and connectors used. Provide schematics and a description of the method of operation of any team-built signal conditioning electronics. Explain how your design meets all of the requirements of FH Rules **IC1.6** and **EV3.5**.

The throttle position sensor consists of two 5k piston potentiometers (figure 20). They are mechanically linked in parallel and will actuate over the same range. The pedal is mechanically limited to 90% of the potentiometer travel range for open/short detection. The first pot (APPS1) is biased from 5-10 volts and the second pot (APPS2) is biased from 0-5 volts. In order to detect open/short circuit conditions APPS2 is passed through a window comparator with a valid range of 0.25-4.75, similarly, APPS1 has the 5 volt bias removed and is passed through a window comparator with the same range. In order to detect throttle plausibility, the biased APPS1 and APPS2 signals are passed through a differential amplifier. The output of the diff-amp is then passed through a window comparator with valid range of 4.5-5.5 volts. This range tolerates up to a 10% difference between APPS1 and APPS2. All of the comparator outputs are tied to a NAND gate. If all comparators have logic high outputs the NAND gate sets the throttle plausibility signal low, allowing the throttle signal from APPS2 to pass through an isolator and then be sent to the motor controller.

Actuator / Encoder manufacturer and model:	LPPS Linear Potentiometer – LPPS-050	
Encoder type (e.g.Potentiometer):	Potentiometer	
Output:	5V range of signals (max 5-10V)	
Is motor controller accelerator signal isolated from TSV?	⊠Yes / □ No	
If no, how will you satisfy rule <b>EV3.5</b> ?	NA	

Table 16 - Throttle Position encoder data

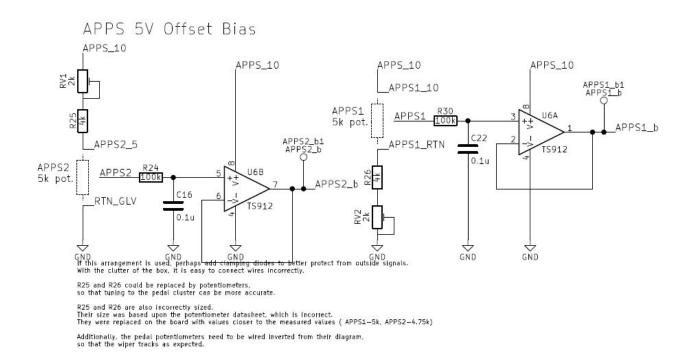


Figure 20 Throttle biasing circuit (From piston potentiometers)

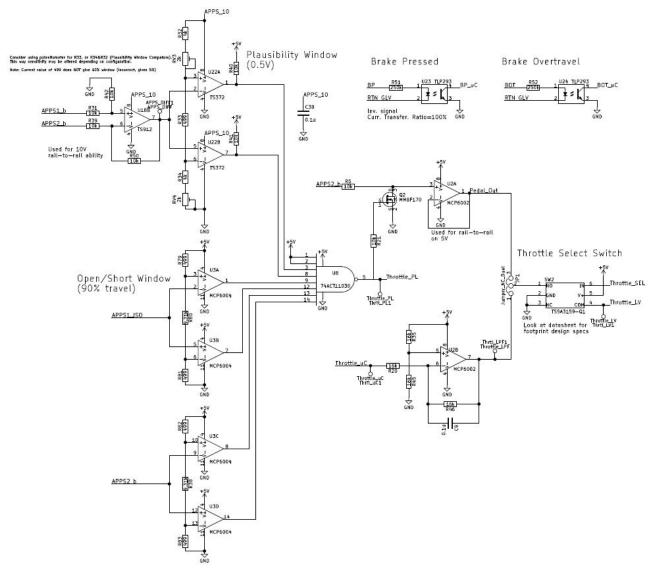


Figure 21 Throttle Plausability Window Check (Click Here for more details)

## 4.8 Accelerator / throttle position encoder error check

Describe how the system reacts if an error (e.g. short circuit or open circuit or equivalent) is detected. Describe circuitry used to check or condition the signal going to the motor controller. Describe how failures (e.g. Implausibility, short circuit, open circuit etc.) are detected and how the system reacts if an error is detected. State how you comply with **EV3.5.4.** 

If a throttle plausibility error is detected, the NAND gate outputs a logic high. This output is tied to the gate of a power MOSFET, and ties the throttle input to the motor controller to 0 volts. The low voltage throttle signal is isolated from the motor controller through the use of a Broadcom

ACPL-C870 optical isolator. The plausibility signal goes to the microcontroller which takes the system out of drive mode.

# Section 5

# **Accumulator System**

Name:	Waseh Ahmad
e-mail:	ahmadw@lafayette.edu

#### **5.1 Accumulator Pack**

Person primarily responsible for this section:

Provide a narrative design of the accumulator system and complete the following table.

The Tractive System Voltage is provided by four accumulator containers placed in series to provide the power necessary to operate the motor. An accumulator segment, housed within each container, is comprised of a battery of 7 LiFeP04 cells (3.2 V nominal) connected in series. Each cell is monitored for temperature and voltage by an AMS (accumulator), which communicates this information to the Pack Management Computer (PacMAN). The PackMAN utilizes an AT90CAN128 Atmel microcontroller.

The accumulator high current output is available through Amphenol PowerLok Connectors. Accumulator voltage is present only while the safety loop is closed. A low current output is also available through an Anderson Power connector. This output is limited to 20 A. Charging is also accomplished through this connector, and is similarly limited to 20 A and 30 V, and implements "plug and forget" charging. The functioning of both ports is controlled by the PackMAN board.

Maximum Voltage (during charging):	96 VDC	
Nominal Voltage:	89.6 VDC	
Total number of cells:	28	
Cell arrangement (x in series / y in parallel):	28 in series	
Are packs commercial or team constructed?	□Commercial / ⊠ Team	
Total Capacity (per FH Rules <b>Appendix A</b> <sup>3</sup> ):	3.6 kWh	
Maximum Segment Capacity	4.05 MJ	
Number of Accumulator Segments	4 (#)	

Table 17 - Main accumulator parameters

<sup>&</sup>lt;sup>3</sup> This includes an 80% derating for available traction energy

Describe how pack capacity is calculated. Provide calculation at 2C (0.5 hour) rate? How is capacity derived from manufacturer's data? If so, include discharge data or graph here. Include Peukert calculation if used (See FH Rules **Appendix A**)

 $Cp = (I^k)^*t = (3^1.05)^*20 = 63.4 AH$ 

 $63.4 = (I^1.05)*0.5$ 

I = 100.686 (half hour discharge)

2C = 50.3 AH

Capacity =  $V_{nom}Ah(0.8)=3.2*28*50.3*0.8$ Segment Capacity = 3.2\*50.3\*7\*3.6=4.05

Show your segment energy calculations. The segment energy is calculated as

V nom x Cell AH (2C rate) x Number of Cells x 3.6 (kJ)

(The 80% factor is not applied for this calculation.)

# 5.2 Cell description

Describe the cell type used and the chemistry and complete the following table.

Cell Manufacturer and Model	AA Portable Power Corp, LFP-G60
Cell type (prismatic, cylindrical, pouch, etc.)	⊠Yes / □ No
Are these pouch cells	□Yes / ⊠ No
Cell nominal capacity at 2C (0.5 hour) rate:	50.3 Ah
Data sheet nominal capacity	60 Ah at 1C rate
Maximum Voltage (during charging):	3.42 V
Nominal Voltage (data sheet value):	3.2 V
Minimum Voltage (AMS setting):	2.7 V
Maximum Cell Temperature (charging - AMS setting)	60 °C

Maximum Cell Temperature (discharging - AMS setting)	60 °C
Cell chemistry:	LiFePO4 in prismatic case

Table 18 - Main cell specification

IMPORTANT: Show your calculations here for 2C nominal AH capacity if the data sheet uses a different discharge rate. Refer to FH rules **Appendix A** 

# 5.3 Cell configuration

Describe cell configuration, show schematics, cover additional parts like internal cell fuses etc. Describe configuration: e.g., N cells in parallel then M packs in series, or N cells in series then M strings in series.

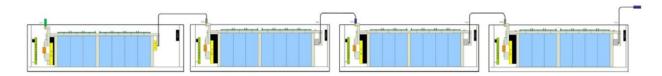


Figure 22 Cell Configuration

In each accumulator segment, seven cells are placed in series. Each segment is within an accumulator container. There are four containers, each of which is placed in series. In total, seven cells in four containers are all in series i.e. 28S1P configuration.

Does the accumulator combine individual cells in parallel without cell fuses?  $\square$  Yes /  $\boxtimes$  No If Yes, explain how **EV2.6** is satisfied.

## **5.4 Segment Maintenance Disconnect**

Describe segment maintenance disconnect (SMD) device, locations, ratings etc.

The SMD consists of Amphenol PowerLok right angled connectors from one segement (pack) to the next as shown in the drawings of section 5.12

Is HVD used as an SMD?	⊠Yes / □ No
Number of SMD Devices / Number of Segments	[ 5 ]/[ 4 ]
SMD MFR and Model	Amphenol PL28W-301-70 PL28X-301-70

	PL00W-301-10D10 PL00X-301-10D10
SMD Rated Voltage (if applicable)	1000 V
SMD Rated Current (if applicable)	250 A (continuous; used with 2/0 cabling which according to Appendix E, have a current capacity of 300 A)
Segment Energy (6 MJ max <sup>4</sup> )	4.05 MJ
Segment Energy Discharge Rate (Ref FH Rules <b>Appendix A</b> )	2 C

Table 19 - SMD Data

#### 5.5 Lithium-Ion Pouch Cells

The vehicle accumulator uses individual pouch cells.

Yes □ No ⊠

Note that designing an accumulator system utilizing pouch cells is a substantial engineering undertaking which may be avoided by using prismatic or cylindrical cells.

If your team has designed your accumulator system using individual Lithium-Ion pouch cells, include drawings, photographs and calculations demonstrating compliance with all sections of rule **EV11**. If your system has been issued a variance to **EV11** by the Formula Hybrid rules committee, include the required documentation from the cell manufacturer.

# 5.6 Cell temperature monitoring

Describe how the temperature of the cells is monitored, where the temperature sensors are placed, how many cells are monitored, etc. Show a map of the physical layout. Provide schematics for team-built electronics.

<sup>&</sup>lt;sup>4</sup> Note Segment energy = rated AH x nominal voltage. The 80% derating is NOT applied for this calculation.

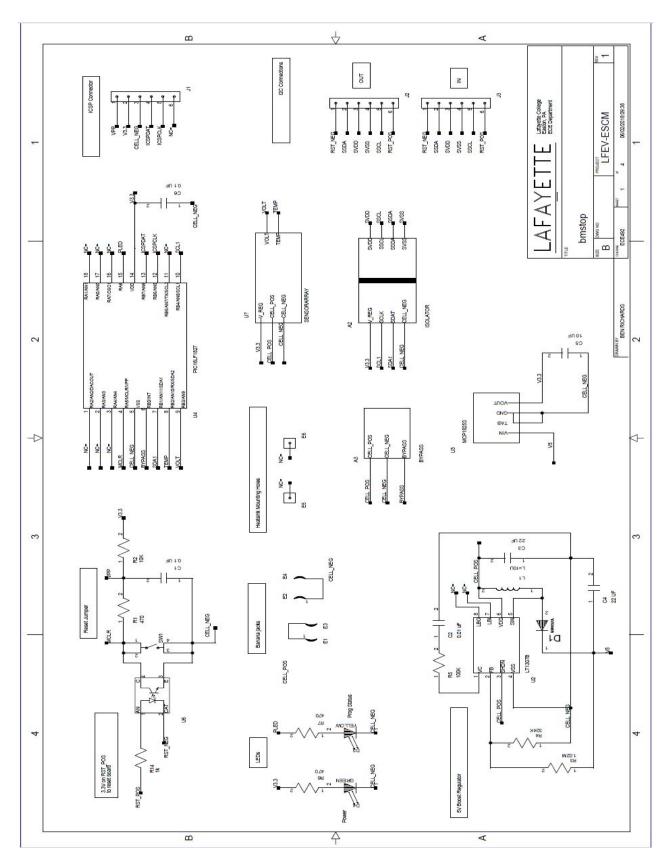


Figure 23 AMS Boards Schematic

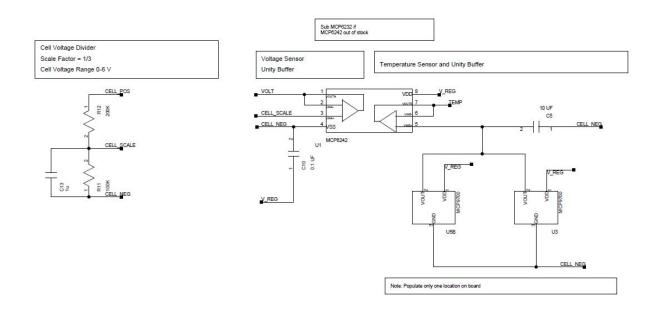


Figure 24 AMS Voltage/Temp monitoring schematic

The above two diagrams are taken from the schematics of the AMS board placed on top of each cell.

Each cell within each accumulator segment is monitored by an AMS board. Each AMS board contains a linear active thermistor (MCP9700, Microchip) that measures the temperature of each cell. The AMS boards communicate this information via I2C to the PacMAN board within their respective accumulator containers, which determines if any cell has exceeded 60° C. If this is the case, a fault case is asserted and the safety loop is opened.

Figure 25 shows the configuration of AMS boards attached to each individual cell.

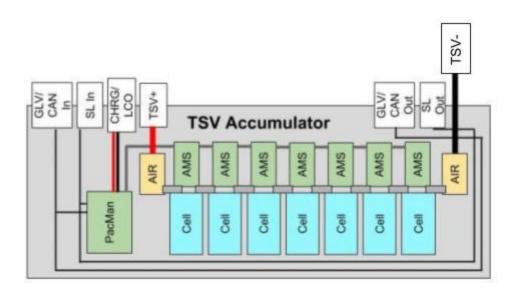


Figure 25 Pack With Cell Config

Number of Cells with Temperature Monitoring (#1)	28
Total Number of Cells (#2)	28
Percentage Monitored (#1 / #2)	100%
Percentage Required by FH Rules: Table 11	30%
If each sensor monitors multiple cells, state how many:	N/A

Table 20 - Cell Temperature Monitoring

# 5.7 Accumulator Isolation Relays (AIR)

Describe the number of AIRs used and their locations. Also complete the following table.

MFR & Model	Gigavac GX14CB	
Contact arraignment:	Single Pole Single Throw Normally Open	
Continuous DC current rating:	350 A	
Overload DC current rating:	1000 A for 85 sec	

Maximum operation voltage:	32 VDC	
Nominal coil voltage:	24 VDC	
Normal Load switching:	Make and break up to 600 A	

Table 21 - AIR data

# 5.8 Accumulator Management System (AMS)

Describe the AMS and how it was chosen. Describe generally how it meets the requirements of **EV2.11.** 

The AMS within each accumulator consists of one PacMAN board and seven AMS boards. The PacMAN board is comprised of a microcontroller (Microchip Technology, AT90CAN128-16AUR) which monitors overall pack current and voltage directly and receives individual cell information from the AMS boards. Each AMS board monitors a single cell for temperature and voltage and communicates this to the PacMAN via I2C. If the PacMAN detects a fault, defined as cell temperature exceeding 60°C, cell voltage exceeding 3.6 V, accumulator segment voltage exceeds 26 V, or an AMS board is unresponsive, the PacMAN board opens the safety loop relay which opens the airs. Accumulator voltage is only present when the safety loop is closed.

PacMAN also keeps track of accumulator state, state of charge, and the state of the safety loop relay on PacMAN. All of these data are regularly sent via CAN frames to the VSCADA computer. The microcontroller communicates on the CAN bus through a Microchip MCP2551 CAN interface IC. This information is also displayed on the top of each accumulator container through the control panel. Managed by PacMAN, this LCD will be able to display pack voltage, pack current, cell voltage, cell temperature, state of charge, cell balancing state, charging state, charging history, discharge history and safety loop state. It will also have functionalities of going into sleep mode and choosing calibration factors where they are necessary.

When either the charging or low current output port (Anderson Power connector on the control panel that is limited to 20 A and 30 V), are in use, a relay on the PacMan computer closes allowing access to the positive and negative terminal of the accumulator. These connections are fused at the terminals with 25A blade fuses. Current flowing through the charge relay also flows through a 1 mOhm current sensing resistor that is monitored via a Kelvin connection by a Texas Instruments INA 226 current monitor. This IC also allows voltage sensing for the full accumulator voltage.

While charging, the voltage of each cell is monitored by the AMS boards, and communicated to PacMAN via I2C. A cell will be placed in bypass mode when its voltage reaches 3.4 V, allowing other cells to continue to charge without overcharging. This is accomplished by allowing some current to pass through a resistor attached to a heat sink instead of the cell. A 5V fan is allowed to run at all times while charging to maintain the ambient temperature inside the accumulator. Once every cell reaches 3.4 V, charging is considered complete. Both bypassing and completion of a

charge cycle trigger an entry in a charge history stored on the microcontroller. This data will be accessible in debug via USB, and an abbreviated history is available on the control panel LCD.

Isolation between TSV and GLV is on the pack manager board with the use of DC/DC converter and opto-isolator.

AMS MFR and Model	Manufactured/Designed in House
Number of AMSs	4 (1 per segment, includes 7 cell monitoring boards and 1 Pack manager)
Upper cell voltage trip	3.6 V
Lower cell voltage trip	2.7 V
Temperature trip	60 °C

Table 22 - AMS Data

- Describe other relevant AMS operation parameters.
- Describe how many cells are monitored by each AMS board, the configuration of the cells, the configuration of the boards and how AMS communications wiring is protected and isolated.
- Describe how the AMS opens the AIRs if an error is detected
- Indicate in the AMS system the location of the isolation between TS and GLV

The isolation is in the PACMan board which uses a DC/DC converter and an optoisolator. Each PACMan only sees at max 24V.

# 5.9 Accumulator wiring, cables, current calculations

Describe internal wiring with schematics if appropriate. Provide calculations for currents and voltages and show data regarding the cables and connectors used. Discuss maximum expected current, DC and AC, and duration Compare the maximum values to nominal currents

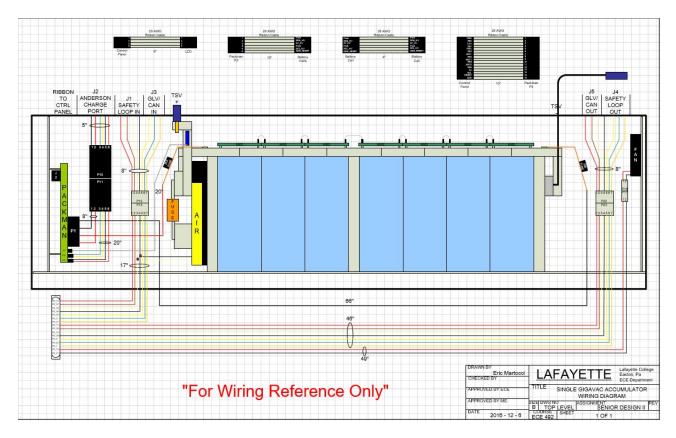


Figure 26 Wiring for one Accumulator Segment

The diagram above shows the wiring for one of the Accumulator Segments.

We expect no AC voltage. For an accumulator container we expect a thevenin voltage of 23.6 V with 14 mOhm thevenin resistance at 100% state of charge. With a fully charged accumulator container, we expect roughly 24 V with seven cells charged to 3.4 V. With a fully charged accumulator system we expect 96 V. From experimentation, it takes 53 minutes for full discharge for a single accumulator container. The low current output draws 20 A. Each cell has 60A-h for 1C.

Through a motor and controller characterization, the maximum RPM is 4500 RPM with a maximum possible torque of 92 ft-lbs. The maximum efficiency motor speed in the fully integrated car is 2500 RPM with steady state torque estimate of 15 ft-lbs based upon a constant power experiment showing the maximum efficiency for the motor reached at and above 2500 RPM. At this maximum efficiency, the motor will draw 71 A from the accumulator. This means the battery will dissipate from this analysis in 51 minutes or 0.85 hours.

The DC current from the accumulator is measured utilizing a current sensor from each accumulator container.

For the rate of charge and discharge of an accumulator container, assuming the slowest possible discharge current for an accumulator at 20A, the actual current is expected to be within the range of 20.366 and 19.634A. Given an accumulator capacity of 60 Ah, the capacity in Coulombs is equal to 216000. At 20 Coulombs per second, the pack will discharge in 10800 seconds, meaning a

discharge rate of 1% every 108 seconds. For 20.366 and 19.634 A, the pack discharges 1.018% or 0.982% every 108 seconds respectively. .018 multiplied by 100 to account for the possible accumulation of error gives a confidence interval of +/ 1.8% between the measured and expected values for state of charge.

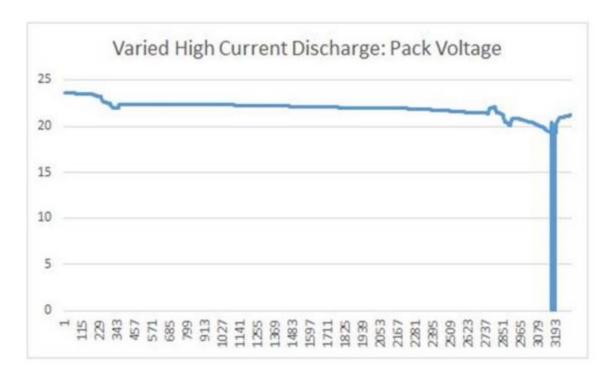


Figure 27 High Current Discharge for Pack

The connectors used are Amphenol PowerLok 300 Series connectors (Section 5.4), with 2/0 fully Shielded cables.

#### 5.10 Accumulator indicator

If accumulator container is removable, describe the indicator, including indicating voltage range

Our Accumulator container is divided into 4 segments, each with a max voltage below 30V. The TSAL light will thus be used as an indicator of the Accumulator, meeting the requirement of turning on when TSV exceeds 32V.

#### 5.11 Charging

Describe how the accumulator will be charged. How will the charger be connected? How is the accumulator to be supervised during charging? Include a diagram showing how the charging circuit is fused.

This design utilizes coulomb counting, integrating the current flowing through the current sensing resistor to determine the increase in state of charge due to charging as well as the decrease in state of charge due to low current output and the operation of the PacMan computer.

To monitor current flowing through the high current output, an Ametes BBM01 current sensor is attached to the 0.5 in by 1 in aluminum bar wire that attaches the negative accumulator terminal to the negative terminal of battery of cells. This sensor provides a differential voltage output that is available to the microcontroller over I2C through a Texas Instruments ADS1115 analog to digital converter.

While charging, the voltage of each cell is monitored by the AMS boards, and communicated to PacMAN via I2C. A cell will be placed in bypass mode when its voltage reaches 3.4 V, allowing other cells to continue to charge without overcharging. This is accomplished allowing some current to pass through a resistor attached to a heat sink instead of the cell. A 5V fan is allowed to run at all times while charging to maintain the ambient temperature inside the accumulator. Once all cells reaches 3.4 V, charging is considered complete. This allows for plug-and-forget charging. Both bypassing and completion of a charge cycle trigger an entry in a charge history stored on the microcontroller. This data will be accessible in debug via USB, and an abbreviated history is available on the LCD.

When the charge relay is closed in figure 28 with the use of the CHRG\_CTRL signal, charge+ feeds into Pack +, which is then protected by a 5A fuse as shown in figure 29.

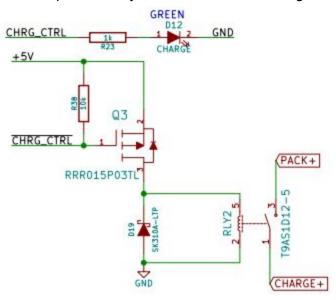


Figure 28 Charging Ciruit

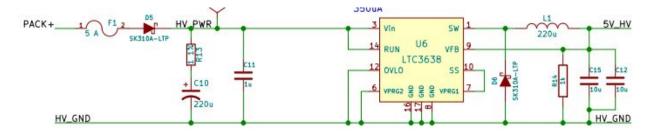


Figure 29 Charging Circuit with Fusing

#### Complete the table

Charger Manufacturer and model:	TDK-Lambda, GenH30-25
Maximum charging power:	0.75 kW
Isolation	⊠Yes / □ No
UL Certification (If "no", fill in the line below)	⊠Yes / □ No
Do you have a waiver from the FH rules committee?	□Yes / □ No
Maximum charging voltage:	30 V
Maximum charging current:	25 A
Interface with accumulator (e.g. CAN, relay etc)	Anderson Charging Port
Input voltage:	85-265 VAC continuous
Input current:	9.5 A

Table 23 - Charger data

## **5.12 Accumulator Container/Housing**

Describe the design of the accumulator container. Include the housing material specifications and construction methods. Include data sheets for insulating materials. Include information documenting compliance with UL94-V0, FAR25 or equivalent.

If the housing is made of conductive material, include information on how the poles of the accumulators are insulated and/or separated from the housing, and describe where and how the container is grounded to the chassis.

Include additional photographs if required to comply with rule EV2.4.

Show how the cells are mounted, use CAD-Renderings or sketches and include calculations showing compliance with FH Rules **EV2.5**.

The cells are mounted within the individual segments of the container. The cells are shown in figure 30 and 31 below. The cells are connected in series using aluminium bars. They are packed together using GLV grounded aluminium bars on the sides (as shown in the figures) and across the top rim of the cells.

The accumulator container will be made of 1/8" Al sheet/plate and each (2) will contain 2 battery packs. The wires are connected to the poles of the accumulators and are encased in an insulated casing. That entire accumulator container will go in the side pods on the car, the area designated for the storage of the packs. The segments are fastened to the car using 5/16-8 grade 5 bolts, 8 per segment, directly to the frame of the car. There will also be cutouts for small amounts of air to help cool the accumulators, although the cells don't end up reaching that high of a temperature during discharge. There will also be through-holes for the mounting method for the battery packs and accumulator containers.

#### Requirements for V-0

- 1. The specimens may not burn with flaming combustion for more than 10 seconds after either application of the test flame.
- 2. The total flaming combustion time may not exceed 50 seconds for the 10 flame applications for each set of 5 specimens.
- 3. The specimens may not burn with flaming or glowing combustion up to the holding clamp.
- 4. The specimens may not drip flaming particles that ignite the dry absorbent surgical cotton located 300 mm below the test specimen.
- 5. The specimens may not have glowing combustion that persists for more than 30 seconds after the second removal of the test flame.

1/8" steel sheet/plate will fulfill the requirements above

The figures below show the accumulator segment containers (at different viewpoints) with the cells.

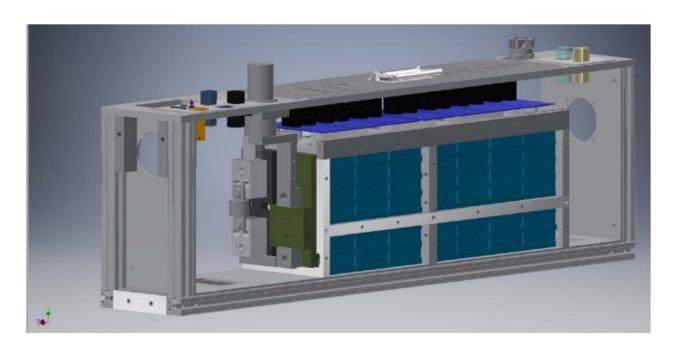


Figure 30 Pack Container View with cells

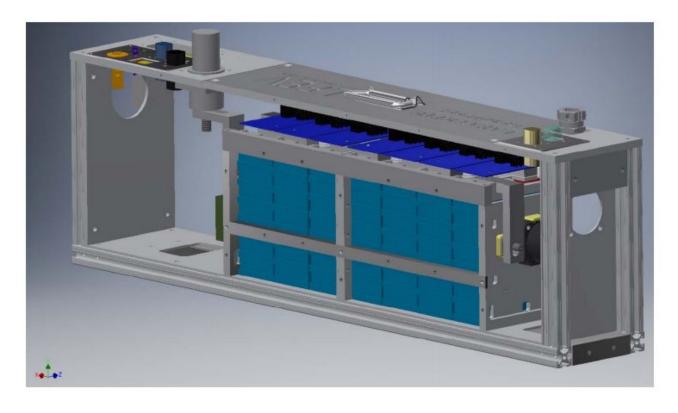


Figure 31 Pack Container View 2 with cells

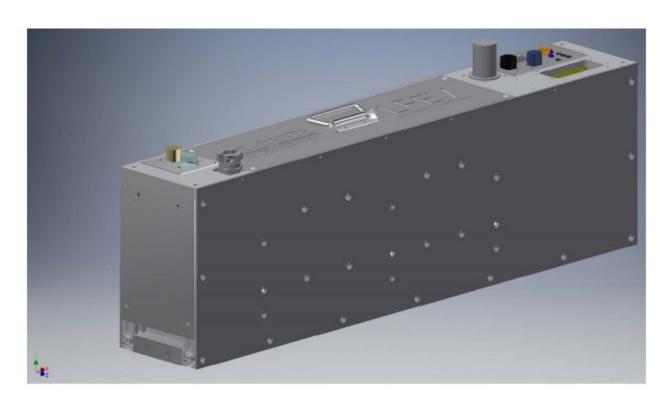


Figure 32 Pack Container Fully assembled container
Section 6

# **Safety Controls and Indicators**

# 6.1 Shutdown Circuit

Include a schematic of the shutdown circuit for your vehicle including all major components in the loop

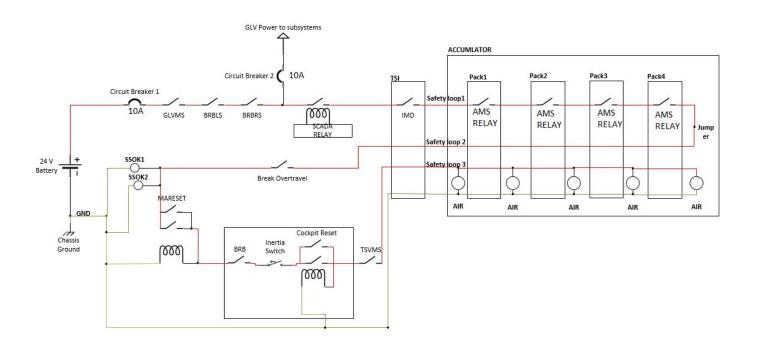


Figure 33 Shutdown Safety Circuit Schematic

Describe the method of operation of your shutdown circuit, including the master switches, shut down buttons, brake over-travel switch, etc. Also complete the following table

Master switches and BRB's shut down entire system. SCADA monitoring, Cooling, AMS and IMD systems have the ability to shut down AIR's in TSV. Then post AMS the Brake overtravel switch and TSV master switch shut down the AIR's outside cockpit. The only Driver resettable switches are the BRB, inertia switch and CPR located directly before the AIR's.

Function (Momentary, Normally Open or Normally Closed)
--

Main Switch (for control and tractive-system; CSMS, TSMS)	Normally Closed	
Brake over-travel switch (BOTS)	Push pull switch that will be pressed when the brake lines do not create enough pressure to stop the pedal. This will stop voltage from reaching the motor controller throttle input. Normally Closed.	
Shutdown buttons (BRB)	Normally Closed	
Insulation Monitoring Device (IMD)	Bender ISOMETER IR155-3203. Operating with normal specs stated on the datasheet. OKHS will be used for monitoring ground 2017 Formula Hybrid ESF (Rev 0C) 42 faults. Normally outputs digital HIGH. Relay Connected is Normally open	
Battery Management System (AMS)	Normally Open Relay	
Interlocks (if used)	N/A	

Table 24 - Switches& devices in the shutdown circuit

Describe wiring and additional circuitry controlling AIRs. Write a functional description of operation

Each accumulator container houses one AIR between the HV positive input terminal of each container and the Mersen/Ferraz Shawmut A3T300 fuse, which then connects to the positive terminal of the first cell in the accumulator segment. Thus, simply, the AIR is in series with the HV input, fuse, and first cell. This AIR in each accumulator container is then connected to the PacMAN board and out the CAN output of the container. Only the first accumulator container in the series contains a second AIR which connects between the minus terminal of the last cell in series in the accumulator segment and the HV negative output terminal of the accumulator container.

If the PacMAN detects a fault, defined as cell temperature exceeding 60°C, cell voltage exceeding 3.6 V, accumulator segment voltage exceeds 26 V, or an AMS board is unresponsive, the PacMAN board opens the AIR. Accumulator voltage is only present when the safety loop is closed. Externally, the AIR can be opened or closed via the CAN connectors on each container from the safety loop

Total Number of AIRs:	5

Coil holding current per AIR:	0.1 A
Current drawn by other components wired in parallel with the AIRs.	0.58 A
Total current in shutdown loop:	1.08 A

Table 25 - Shutdown circuit Current Draw

Provide CAD-renderings showing the shutdown circuit parts. Mark the parts in the renderings

The markings for the system buttons/switches aren't sure

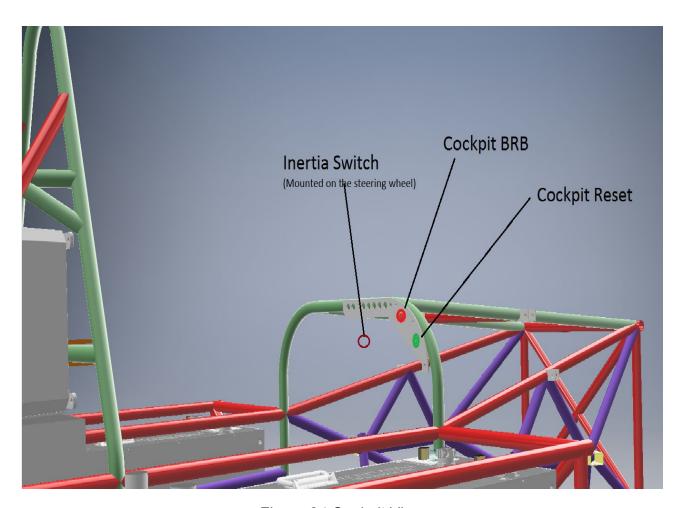


Figure 34 Cockpit View

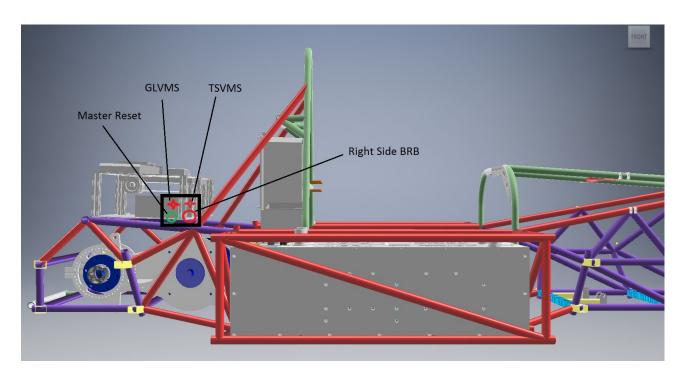


Figure 35 Side View- Shutdown

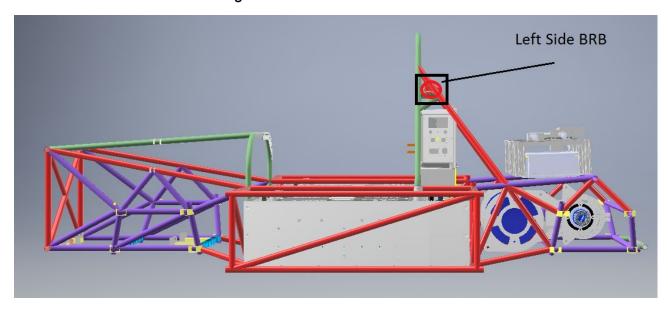


Figure 36 Side View- Shutdown

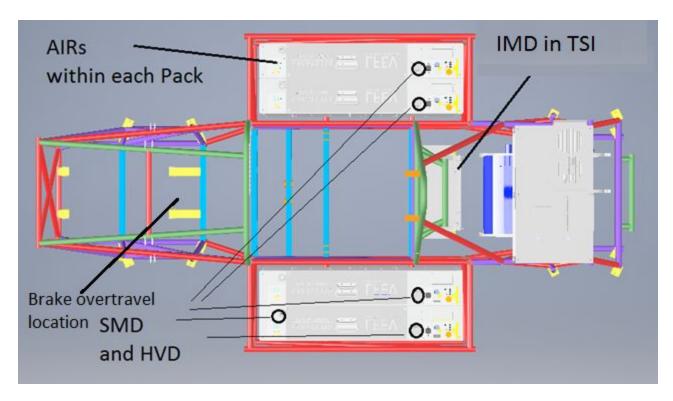


Figure 37 Top View -Shutdown Circuit Components

If your shutdown state diagram differs from the one in the Formula Hybrid rules, provide a copy of your state diagram (commented as necessary).

State Diagram Compliant with Formula Hybrid Rules

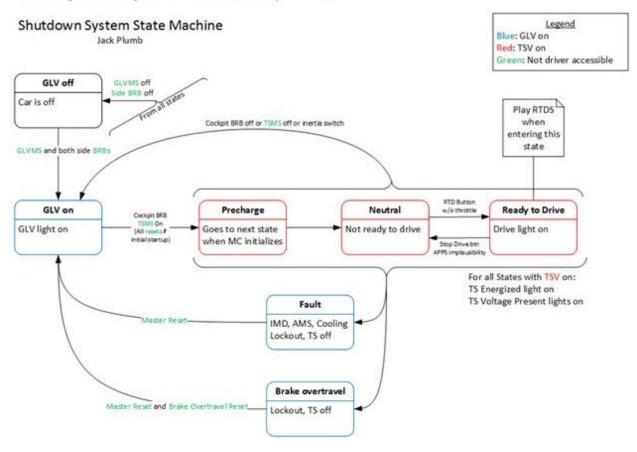


Figure 38 Shutdown State Diagram

#### 6.2 IMD

Describe the IMD used and use a table for the common operation parameters, like supply voltage, temperature, etc. Describe how the IMD indicator light is wired. Complete the following table.

MFR / Model	Bender ISOMETER IR155-3203
Set response value:	100 kΩ (1KΩ/Volt)

Table 26 - Parameters of the IMD

Describe IMD wiring with schematics.

The IMD is connected directly to the HV source within the TSI. It has 3 connections to GLV gnd as well as one connection to the 24V GLV. One connection goes to the IMD relay which is normally open. This relay has control over the safety loop. The last connection is the IMD\_PWM signal from a microcontroller in the TSI. Refer to figure 9 for details regarding the IMD wiring.

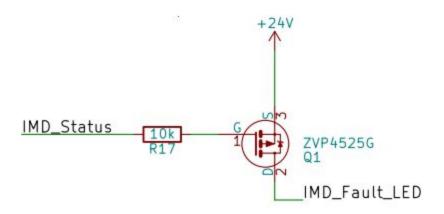


Figure 39 IMD Indicator LED Circuit

The IMD Status is fed into the TSI board from the IMD. This signal then uses a mosfet switch to control the IMD\_FAULT\_LED as shown in the figure 35 above.

# 6.3 Reset / Latching for IMD and AMS

Describe the functioning and circuitry of the latching/reset system for a tripped IMD or AMS. Describe wiring, provide schematics.

The IMD tripped circuit will open a relay that is use to complete the safety loop. When the OKHS signal is not producing the normal 24V during safe usage, the relay will open and the override button that is not driver resettable will need to be pushed in order to close this relay again.

When AMS or IMD breaks the safety loop two reset buttons must be pushed to re-engage the AIR's. The Master reset on the outside of the car and the CPR in the cockpit of the car. Both are latching buttons. By pressing the reset it shorts the second switch and provides current through the inductor closing the bottom switch. Refer to figure 33 for a schematic of the wiring for the reset button.

The IMD interface can be seen in figure 9. The IMD is connected to the TSI board which has internal connections to the IMD relay. The following diagram shows IMD connected to an OMRON 24V DC relay. The safety loop passes through this relay and then through the 4 segments of the accumulator, each containing an OMRON SPST relay. The final relay then connects to the Master reset switch as shown in figure 33 (did not include brake over travel in the circuit below). The reset switch is normally open and held closed by the coil. When the safety loop opens due to the IMD or AMS fault, current ceases to pass via the coil, opening the switch. The switch is located behind the driver, close to the BRB-RS. The switch therefore acts as the latch.

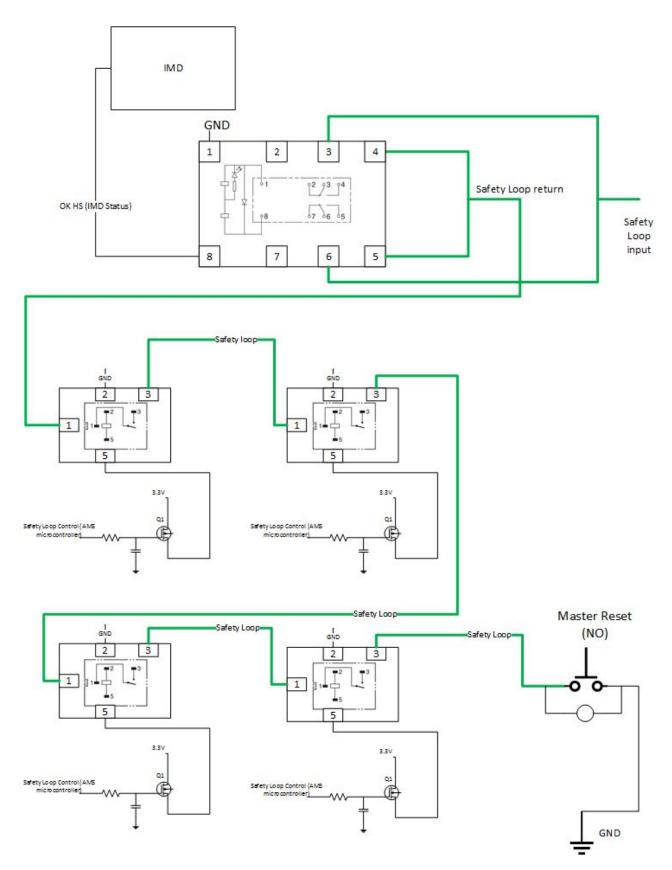


Figure 40 Latching/reset Circuit

# 6.4 Shutdown System Interlocks

(If used) describe the functioning and circuitry of the Shutdown System Interlocks. Describe wiring, provide schematics.

N/A

# 6.5 Tractive System Active Lamp (TSAL)

Describe the tractive system active lamp components and method of operation. Describe location and wiring, provide schematics. See **EV9.1.** 

The red TSAL will be connected to the TSV via the TSI. Once the AIRS are closed, the TSI has access to the TSV. The voltage will pass through a DC/DC converter on the TSI PCB to provide power to the TSAL lamps as shown in the figure 41 below. As the system has been configured to open the safety loop if voltage goes below 80V and the voltage the light turns on at is 27V, the 32V min voltage requirement is met (where the light must be on if voltage exceeds 32 V in TS). The TSAL will also flash at a rate of 2-3 Hz.

There has been a change in the schematic a bit and there is no longer a voltage divider. Therefore, the TSAL lamp will now turn on for any voltage greater than 16V. This can be shown by the minimum input voltage for the DC/DC converter (of 16V) (RUW15L12C datasheet).

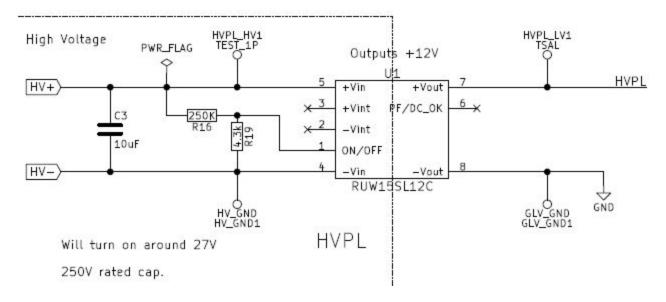


Figure 41 TSAL Wiring in the TSI

The TSAL will be located under the highest point of the main roll hoop.

# 6.6 Safety Systems OK Lamp (SSOK)

Describe the Safety Systems OK Lamp components and method of operation. Describe location and wiring, provide schematics. See **EV9.3** 

The SSOK Lamps are Amber and comply with DOT FMVSS 108. The position can be seen relative to other systems in section 6.1 figure. They are powered by a 12V supply from the GLV via a diode.

GLV Master Switch
Both side-mounted shutdown buttons (BRBs)
Brake over-travel switch
Accumulator Monitoring System (AMS)
Insulation Monitoring Device (IMD)
Master Reset (MARSET)

Refer to Section 6.1 for position of SSOK in the safety loop.

### 6.7 Ready-To-Drive-Sound (RTDS)

Describe your design for the RTDS system. See EV9.2.

The ready to drive sound will activate when the drive button is pressed assuming the correct startup sequence has been met up to that point. This information will be made available to us by the VSCADA system over CAN bus. If all conditions are met when the button is pressed, the microcontroller used in the TSI system will drive a sound maker similar to the provided sound clips for 2 seconds.

Section 7

# **GLV System**

Name:	Waseh Ahmad	
e-mail:	ahmadw@lafayette.edu	

# 7.1 GLV System Data

Person primarily responsible for this section:

Provide a brief description of the GLV system and complete the following table

The GLV system is comprised of the 24V LiFePo4 battery, vehicle computer interface (VCI), the vehicle user interface (VUI) and the safety loop. The battery provides 24V to all sub-systems. The VCI provides hardware for VSCADA interfacing. The VUI is the driver interface including buttons and dashboard display screen. The safety loop assures all systems are functioning properly before opening airs and allowing HV from the accumulators.

GLV System Voltage	24V
GLV Main Fuse Rating	10A
Is a Li-lon GLV battery used?	⊠Yes / □ No
If Yes, is a firewall provided per <b>T4.5.1</b> ?	⊠Yes / □ No
Is a dc-dc converter used from TSV?	□Yes / ⊠ No
Is the GLV system grounded to chassis?	⊠Yes / □ No
Does the design comply with <b>EV4</b> ?	⊠Yes / □ No

Table 27- GLV System Data

Section 8

# **Appendices**

Include only highly-relevant data. A link to a web document in the ESF text is often more convenient for the reviewer.

The specification section of the accumulator data sheet, and sections used for determining accumulator capacity (FH Rules **Appendix A**) should be included here.

#### Cell MSDS

http://www.batteryspace.com/prod-specs/MSDS/2015/MSDS-LFP-G60%20ECO%202015.pdf