# Bushkill Creek Survey Report 3<sup>rd</sup> Street to the PA Route 22 Overpass



CE 421 Hydrology Class Prof. David Brandes Dept of Civil & Environmental Engineering Fall 2010 Last Revised June 04, 2011

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## 1. Background

The purpose of this report is to provide the necessary base mapping for the continued analysis of the Bushkill Creek low-head dam on Lafayette College owned property near 3<sup>rd</sup> Street in the city of Easton. The feasibility of this structure to provide hydro-power to the existing buildings in the immediate area was previously evaluated in the spring of 2009 and a report of those findings is available through the Department of Civil and Environmental Engineering. It appears, based on the aforementioned report, that a project utilizing hydropower at this location is neither economically or technically feasible based on currently available technologies.

Therefore focus has shifted from utilizing and rehabilitating the existing dam to the removal of the structure. This could be accomplished through the cooperation of private industry with various local and state regulatory agencies including the Pennsylvania Fish and Boat Commission which provides funding for projects similar to this one in both size and scope. This base mapping is being prepared in conjunction with separate reports that will analyze the potential environmental impacts of the removal of this dam, the flood protection which the current dam may or may not provide, and the potential hydraulic impacts to the channel if the dam were removed.

## 2. Site Description

The Bushkill Creek dam is located approximately three hundred feet (300'), west of the bridge at north Third Street in the City of Easton. There are existing structures built over the channel by using concrete piers. The survey of the channel began at the face of the first row of piers and continued to the west. The western limit of the survey is the Pennsylvania Department of Transportation (PennDOT) bridge for Route 22 over the Bushkill Creek and Bushkill Drive / Pearl Street. The total length of surveyed channel is approximately nine hundred feet (900'). *Figure 1* below shows a topographic map of the general project area from a USGS 7.5 minute, 1:24000, Easton PA-NJ quadrangle.



**Figure 1:** Topographic Map of Bushkill Creek

The survey located the edges of existing pavement for Bushkill Drive / Pearl Street. The northern edge of pavement is also the bottom of the embankment at the base of the college campus. This also represents the northern limit of the survey. The southern limit of the survey is the top of the stream embankment adjacent to a recently demolished industrial facility, an existing warehouse, and a recently refurbished parking area. An aerial photograph, from Google Maps, is shown in *Figure 2* below and better depicts the limits of the survey.



**Figure 2:** Aerial Photo of Bushkill Creek

## 3. Methods & Objectives

In order to provide adequate base mapping to support the analyses mentioned in the Background section of this report two types of surveys were conducted. First, a horizontal and vertical traverse was established which encompassed the project area. According to the *Land Surveyor Reference Manual*, "a traverse is a series of lines connecting successive instrument stations of a survey. The relative position of the stations is determined by the direction and length of the lines (Harbin 1989)." The traverse is sometimes referred to as the "control" for a survey. In this case, a particular type of traverse was employed, which is called a closed traverse or loop traverse. Again using the definition from the *Land Surveyor Reference Manual*, "The closed traverse, also called the loop traverse, starts and ends at the same point. Because it is a closed polygon, the interior angles and lengths of the sides may be checked for accuracy and

mathematically adjusted (Harbin 1989)." By using this type of survey the accuracy and precision of the survey can be measured and reported.

The second type of survey conducted at this location if a topographic survey. This is done to create a topographic map or contour map of the area. Referring to the *Land Surveyor Reference Manual,* "Topographic Surveys are made to determine the relative positions of points and objects so that a map maker can accurately represent their positions on the map (Harbin 1989)." Each contour line shown on a topographic map is an imaginary line at the ground surface representing an equal vertical elevation. The contour interval is the vertical distance separating two adjacent contour lines. The most common intervals used for detailed mapping are one and two foot spacing and the one used here is the one foot spacing. This means that each contour line shown on the finished topographic map represents one foot of vertical elevation change. The spacing of the contour lines between one another also gives an indication of how steep the ground slopes. For example the closer these lines are spaced the more steep the elevation change of the ground. The farther apart contour lines are spaced the flatter or more gradual the ground slope.

## 4. Horizontal & Vertical Control Survey

The control loop was started at a nail set along the southern edge of pavement of Bushkill Drive / Pearl Street. This point was also located just north of the existing dam. The first back-sight was established at the intersection of Bushkill Drive with North Third Street. A radial control point was established in a concrete structure on the north side of the existing dam and overlooking the area. The next control point was established travelling west and set near the northern edge of pavement of Bushkill Drive / Pearl Street and to the east of an existing two-story residential dwelling. A radial control point was established in a concrete structure along the north side of Bushkill Creek with a view of the island below the Route 22 overpass. The next control point, travelling south and west was established at the intersection of Bushkill Street with Pearl Street and sighting under the Route 22 overpass structure. This point was set in the Bushkill Street Bridge over the creek. The next control point was established travelling east along Bushkill Street on the northeast corner of the Route 22 off-ramp. The next control point was established travelling east along Bushkill Street at the northwest corner of the intersection with North Third Street. The next control point which was observed was also the first back-sight point located on the northwest corner of the intersection of North Third Street and Bushkill Drive. The last observations were made by occupying this control point and closing the traverse to the point of beginning at the first control point.

The Horizontal and Vertical Control data were recorded in a field book and the corresponding notes are included as *Attachment A* at the end of this report. At each

control station, observations were made direct and inverse to help reduce error. This data was entered into an Excel spreadsheet to determine the average observed angles in both the horizontal and vertical direction. The average horizontal angle was then used as the interior angle of the traverse loop, sometimes referred to as the angle turned. The reduction of this data is shown in the attached spreadsheet as *Attachment B*. A sketch of the raw or unadjusted traverse loop was prepared and is shown as *Attachment C*. The sum of the interior angles for any closed figure with (*n*) number of sides is as follows:

## Sum of Interior Angles = $(n-2) \times 180^{\circ}$

Using the above equation the total horizontal angular error can be determined. The total error for this traverse was calculated to be thirty-six seconds (36"). There are a total of six interior angles for this traverse and the error per control observation is six seconds (6"). The precision of the Topcon total station used for this survey was five seconds (5"). The angular precision for this control survey is within acceptable tolerances. The linear errors of closure were as follows:

	Hz.	Vt.
1-1'	0.037′	0.004'
2-2'	0.027'	0.008'

The total perimeter of the traverse is approximately 2782.664'. According to the *Land Surveyor Reference Manual,*"The ratio of the error, or precision, of a traverse is the ratio of the error of closure to the perimeter. It is expressed with the numerator as one (1) and the denominator in round numbers. It is a measure of the precision of a traverse (Harbin 1989)." In this case the error of closure or ratio of error is as follows:

1-1'	1 / 75,207′
2-2′	1 / 103,676'

This indicates an error of one foot per 75,207 feet in distance. Although these errors indicate a survey with acceptable precision for the sake of completeness the traverse was balanced using the compass rule, sometimes called the Bowditch rule. This method of adjustment is most commonly used and applies when the angular and linear accuracies are approximately the same (Harbin 1989). According to the *Land Surveyor Reference Manual*, "Using the compass rule, the difference in the sums of the north and south latitudes is distributed over the latitudes of the traverse. A correction is made in the latitude of each side to bring the north and south latitudes into balance. The difference in the sums of the east and west departures is distributed in the same way (Harbin 1989)."

The equation is shown as follows:

# correction for $AB = \frac{\text{dif in lat}}{\text{perimeter}} \times \text{length } AB$

The traverse loop was adjusted based on the above equation in both the north-south (latitudes) and east-west (departures) directions. The Excel Spreadsheet showing these calculations and corresponding corrections is shown as *Attachment D* at the end of this report. These control points were then inserted into an AutoCAD drawing file, specifically Land Development Desktop 2009 edition.

Once inserted it should be noted that the original survey was conducted based on an arbitrary, assumed datum with starting point located at the first established control point with the following coordinate information:

Point #	Northing	Easting	Elevation	Description
1	5,000.00	5,000.00	100.00	PK Nail

This information was then compared with two National Geodetic Survey (NGS) control points KV1684 and KV1464. The NGS data sheets for these two control benchmarks are shown in *Attachment E* at the end of this report. The Northampton County GIS department aerial photograph was then imported into the drawing. This mapping is based on the Pennsylvania State Plane – South Zone Coordinate system. Once inserted the positions of the two control points were located based on the arbitrary survey and the desired coordinate system mentioned above. The survey was then translated and rotated to the aerial photograph as accurately as possible.

The vertical benchmark for this survey is the NGS disk located in the east pillar of the entrance gate near the intersection of Bushkill Drive and North Third Street. The datum used is the stamped elevation of 196.217 as established in 1932. It should be noted that according to NGS this survey mark is of questionable or unknown stability because repeated measurements indicate possible vertical movement. The amount of vertical movement described is acceptable for the analyses being conducted on the dam, particularly the hydrologic / hydraulic analyses for which accurate relative elevations, (i.e. elevation difference), are required rather than absolute elevations. Therefore the elevation as marked on the stamped brass disk is being used and held as the vertical control benchmark for the survey.

The method employed here does not guarantee the accuracy of the control points or survey to within survey grade precision of the State Plane Coordinate system; however the values of the observed survey positions and their relative location based on the aerial photograph were extremely close to one another. The control points listed in the coordinate index and shown as *Attachment F* at the end of this report are within a reasonable tolerance for the analyses being conducted on the existing dam.

## 5. Topographic Survey

The topographic survey was conducted on July 16, 22, and 23, 2010. Additional data was collected on November 6, 2010. Cross sections of the channel were located at approximately fifty-foot (50') intervals. All defining features of the channel were located including edges of pavement along Bushkill Drive and Pearl Streets, top and bottom of embankment, several shots along the bottom of the stream bed, the island was located to the north and east of the Route 22 overpass, and the piers and parapet walls of the existing bridge were located. Measurements were taken to define the geometry of the dam, spillway, and concrete apron downstream of the structure. The piers of the existing buildings at North Third Street were also measured.

This information was collected using a TDS data collector / data logger. The raw data was imported into the control survey. The points were then used to create a topographic map with one foot contour intervals. The complete point file of all the data points is shown as *Appendix G* of this report. The complete topographic map showing the locations of the cross section generated for the data analysis of the existing dam structure is shown as *Appendix H* of this report. Vertical centerline profiles were generated from the base topographic mapping and are shown in the following *Appendices*:

Appendix I:	Centerline Profile of Bushkill Creek through Center of Island
Appendix J:	Centerline Profile of Bushkill Creek Main Channel around the
	North Side of the Island
Appendix K:	Centerline Profile of Bushkill Creek Secondary Channel around the
	South Side of the Island

Finally, the above mapping was combined into one sheet consisting of two plan views, one with an aerial photograph overlay and one without, and all three profile views. An exhibit size, not to scale, version of this drawing is shown in *Appendix L* at the end of this report. A full size, 24"x36" scaled copy of the same sheet is included in a separate folder at the back of this report.

## 6. References

Harbin, Andrew L. (1989). "Land Surveyor Reference Manual." 2<sup>nd</sup> Edition. Professional Publications Inc., Belmont, CA.

7. Appendix A: Field Book Notes





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	199-	50-30	89-40-	55	429.510	2-03	5:00!	PIK
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	19 -	50-45	270-18-	55	429.520	1.3.3	5.00'	inverse
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_	314-0	0-55	270-23	-40	482,000		5.00'04	inverse
_	15-2	4-20	93-33	-15	99.025	6	5.00'	PK-Dan
_	195-2	4-30	266-26	-45	99,005	6-	5.00'	invers

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24.20	180	-00-20	269-43	-15:00	481,955		6.50	inverse
	228	-42-40	271-34	-00	541.495		7.00'	inverse
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STA:	Hz	Vt	Slope	Target	H.T.	Notes
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	90-31-15	90-43-00	508,675	2'	5.00'	pk
1.1.1612 1	180-00-40	270-13-30	497.835	7	5.00'	inverse
	270-31-40	269-16-30	508.660	.2'	5.00'	inverse
⊼@ 2'	B.S. 8					1. 1. 1. E.
HI =	5.245					4
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- 10 - 13	63-59-35	92-02-30 :	288.260	10	5.00	pk64
1997 3	180-00-10	270-40-35	508.645	. 8-	5.00	inverse
1000	243-59-55	267-57-20	288.400	10	5.00	inverse
	00-00-00	89-19-05 A	508.655	. 8	5.00	pk
1.0	66-41-40	91-52-06	323.635	1'	5.00	pk-close
	180-00-15	270-40-35	508.230	8	5.00	inverse
	246-41-50	268-07-40	323.620	1'	5.00	inverse
	31-20-10	92-54-05	18 850	11	5.00	VV1414



Cross-Section Survey Bushkill Creek · Rods checked & Dales: 7/16/2010 calibrated prior to SURVey 7/22/2010 7/23/2010 Party: A. Bernstein M. Thompson M. Conlon Sunny/Warm ~ 85°-90° Notes at 50' intervals along Creek from building piers · Cross Sections measured length of Bushkill to tip of island . TDS Data Collector / Logger used to information record pasition Cross Section Survey · Rods checked & Bushkill Creek calibrated prior to Dates: 11/06/2010 survey Party: W.T. Barlow D. Buckley J. Munson A. Bernstein P. Sunny/P. Cloudy Cool-50° Notes: · Cross Sections measured at 50' intervals along length of Bushleill Creek from tip of island to PA Rovie 22 over pass • In-fill Section upstream of dama possible erroneous point group a verify thecking • TDS Data Logger / Data Collector used to

information.

record position

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7	5.043			111.845	123.928		
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_		-0,958	-4.9375		
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6	101.454					
7	118,865		-			
8	116.387					
1'	99.996					
2'	110.258					
KV1684	134,03					
PK64	100,278					
KV1464	115.724					
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1-1'	H2 Vt					
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# 8. Appendix B: Field Data Reduction

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1	0	0	0	2	199	50	30	199	50	50	88	13	20	+	1	46	40	1	46	35	323.59	323.595	BS	323.439	10.03	+
	199	50	30	3	199	51	10				89	40	55	+	0	19	5				429.51					
	180	0	25	2							271	46	30	+	1	46	30	0	19	0	323.61	429.515	FS	429.508	2.374	+
	19	50	45	3							270	18	55	+	0	18	55				429.52					
3	0	0	0	1	134	0	35	134	0	30	90	20	40	-	0	20	40	0	20	45	429.46	429.463	BS	429.454	2.592	-
	134	0	35	5	134	0	25				89	36	5	+	0	23	55				482.01					
	180	0	30	1							269	39	10	-	0	20	50	0	23	48	429.47	482.003	FS	481.991	3.337	+
	314	0	55	5							270	23	40	+	0	23	40				482					
5	0	0	0	3	48	42	15	48	42	18	90	16	30	-	0	16	30	0	16	38	481.99	481.97	BS	481.964	2.332	-
	48	42	15	7	48	42	20				88	25	50	+	1	34	10				541.47					
	180	0	20	3							269	43	15	-	0	16	45	1	34	5	481.96	541.483	FS	541.28	14.82	+
	228	42	40	7							271	34	0	+	1	34	0				541.5					
7	0	0	0	5	180	13	55	180	14	12	91	17	45	-	1	17	45	1	17	55	541.43	541.443	BS	541.303	12.27	-
	180	13	55	8	180	14	30			_	90	16	35	-	Ó	16	35				497.81					
	180	0	15	5							268	41	55	-	1	18	5	0	16	45	541.46	497.825	FS	497.819	2.426	-
	0	14	15	8							269	43	5	-	Ó	16	55				497.84		lt			
8	0	0	0	7	90	31	15	90	31	8	89	46	0	+	0	14	0	0	13	45	497.86	497.845	BS	497.841	1.991	+
	90	31	15	2	90	31	0				90	43	0	-	l o	43	0				508.68					
	180	0	40	7							270	13	30	+	0	13	30	0	43	15	497.84	508.668	FS	508.627	6.399	-
	270	31	40	2							269	16	30	-	0	43	30				508.66					
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	180	0	15	8							270	40	35	+	Ó	40	35	1 1	52	13	508.63	323.628		323,455	10.56	1-
	246	41	50	1'							268	7	40	-	1 1	52	20				323.62					
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	110	16	5	4	110	15	40				97	50	40	-	7	50	40				44.215					
	180	0	25	2							271	46	30	+	1	46	30	7	50	42	323.61	44.21	FS	43,796	6.034	<u> </u>
	290	16	5	4							262	9	15	-	7	50	45				44.205					
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	180	0	30	1							269	39	10	-	0	20	50	3	33	15	429.47	99.015	FS	98.825	6.138	-
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	246	15	40	KV1684	246	16	15		_		80	15	20	+	9	44	40				168.97					
	180	0	20	3							269	43	15	-	0	16	45	9	44	23	481.96	168.958	FS	166.522	28.58	+
	66	16	35	KV1684							279	44	5	+	9	44	5		1		168.95		ll –			
2	0	0	0	8	63	59	35	63	59	40	89	19	15	+	0	40	45	0	40	40	508.64	508.64	BS	508.604	6.017	+
	63	59	35	PK264	63	59	45				92	2	30	-	2	2	30				288.26			· · · · · ·		
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																	-				1		lt			
								31	20	10	92	54	5	-	2	54	5	1			1	11.11	FS	11.096	0.562	-
								252	24	15	89	17	50	+		42	10	1			1	18.85	FS	18.848	0.231	+
																		1			1		╢╴			
																					1			ΗZ	19.03	

## 9. Appendix C: Raw Traverse Sketch



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# 10. Appendix D: Compass Rule Adjustment

	Bearing	Distance	Lat	Dep	N	E					CORRECTION	S	Lat	Dep	Ν	E	Elev	DESC
2	S45°00'00''W	323.439	-228.706	-228.706	5228.706	5228.706					0.002661749	-0.00162727	-228.7033	-228.7076	5228.7033	5228.7076	110.2500	2
1	S64°50'50''W	429.508	-182.555	-388.781	5000	5000					0.003534646	-0.002160919	-182.5515	-388.7832	5000.0000	5000.0000	100.0000	1
3	S18°51'20''W	481.991	-456.1256	-155.7715	4817.445	4611.219					0.003966556	-0.002424969	-456.1216	-155.7739	4817.4485	4611.2168	102.4150	3
-																		
																	'	
5	N67°33'38''E	541.28	206.6102	500.296	4361.319	4455.448					0.004454477	-0.002723261	206.6147	500.2933	4361.3269	4455.4429	105.7720	5
																	'	
6															 		'	
7	N67°47'50''E	497.819	188.1187	460.9068	4567.93	4955.744					0.004096813	-0.002504602	188.1228	460.9043	4567.9416	4955.7362	118.8650	7
															 		ļ'	
													712.915 101.2351	- APROL 21 (2014)24-24-24				
8	N21°41'02''W	508.627	472.6348	-187.9303	4756.048	5416.65					0.004185758	-0.002558979	472.639	-187.9329	 4756.0644	5416.6405	116.3870	8
							ERRORS	- 200 144							 		ļ'	
							Lat	Dep	-	TOTAL								
2	S45°00'36''W	323.455	-228.677	-228.757	5228.683	5228.72	0.0229	-0.014		0.02684	0.002661881	-0.001627351	-228.6743	-228.7586	 5228.7033	5228.7076	110.2500	2
							-								 		<b> </b> '	
					5000 000	1000 000	0.0004			0.007.100			-		 		<b> </b> '	
1	-				5000.006	4999.963	-0.0061	0.037		0.037499		-			 			
															 		<b> </b> '	
		0700.004		-			6										'	
б. Г.		2/82.664													 		'	
															 		'	
							9	Lat							 		'	
								0.0000082	-0.0000050								I	

#### 11. Appendix E: NGS Data Sheets

#### The NGS Data Sheet

See file dsdata.txt for more information about the datasheet. DATABASE = , PROGRAM = datasheet, VERSION = 7.85 National Geodetic Survey, Retrieval Date = JUNE 30, 2010 1 KV1684 DESIGNATION - J 269 PADH KV1684 PID - KV1684 KV1684 STATE/COUNTY- PA/NORTHAMPTON KV1684 USGS QUAD - EASTON (1994) KV1684 KV1684 \*CURRENT SURVEY CONTROL KV1684 KV1684\* NAD 83(1986)- 40 41 39. (N) 075 12 49. (W) SCALED KV1684\* NAVD 88 ---64.745 (meters) 212.42 (feet) ADJUSTED KV1684 KV1684 GEOID HEIGHT-KV1684 DYNAMIC HT --34.07 (meters) GEOID09 64.715 (meters) 212.32 (feet) COMP KV1684 MODELED GRAV-980,157.4 (mgal) NAVD 88 KV1684 KV1684 VERT ORDER - SECOND CLASS 0 KV1684 KV1684. The horizontal coordinates were scaled from a topographic map and have KV1684.an estimated accuracy of +/- 6 seconds. KV1684 KV1684. The orthometric height was determined by differential leveling and KV1684.adjusted in June 1991. KV1684 KV1684. The geoid height was determined by GEOID09. KV1684 KV1684. The dynamic height is computed by dividing the NAVD 88 KV1684.geopotential number by the normal gravity value computed on the KV1684.Geodetic Reference System of 1980 (GRS 80) ellipsoid at 45 KV1684.degrees latitude (g = 980.6199 gals.). KV1684 KV1684. The modeled gravity was interpolated from observed gravity values. KV1684 KV1684; North Units Estimated Accuracy East MT (+/- 180 meters Scaled) KV1684;SPC PA S 154,180. 814,350. KV1684 KV1684 SUPERSEDED SURVEY CONTROL KV1684 KV1684 NGVD 29 (??/??/??) 64.958 (m) 213.12 (f) ADJUSTED 20 KV1684 KV1684.Superseded values are not recommended for survey control. KV1684.NGS no longer adjusts projects to the NAD 27 or NGVD 29 datums. KV1684.See file dsdata.txt to determine how the superseded data were derived. KV1684 KV1684 U.S. NATIONAL GRID SPATIAL ADDRESS: 18TVL819048 (NAD 83) KV1684 MARKER: DD = SURVEY DISK KV1684 SETTING: 36 = SET IN A MASSIVE STRUCTURE KV1684 SP SET: BRIDGE KV1684 STAMPING: J 269 1960 KV1684 STABILITY: B = PROBABLY HOLD POSITION/ELEVATION WELL KV1684 KV1684 HISTORY - Date Condition Report By

– 1960 MONUL – 1961 GOOD – 20021117 GOOD PADH KV1684 HISTORY MONUMENTED KV1684 HISTORY KV1684 HISTORY CGS USPSQD KV1684 KV1684 STATION DESCRIPTION KV1684 KV1684'DESCRIBED BY COAST AND GEODETIC SURVEY 1961 KV1684'0.5 MI NW FROM EASTON. KV1684'0.5 MILE NORTH WEST FROM WHERE U.S. HY. 22 GOES OVER 3RD. ST. KV1684'IN EASTON, LOCATED ON TOP OF THE SOUTH WEST WINGWALL OF A 200 KV1684'FOOT CONCRETE BRIDGE OVER BUSHKILL CREEK AND BLACKTOP ROAD, 19.5 KV1684'FEET SOUTH OF THE CENTERLINE OF EAST BOUND LANE, 33 FEET SOUTH KV1684'EAST OF THE CENTERLINE OF HY. 22, 66 FEET SOUTH WEST OF METAL KV1684'LIGHT POLE, ABOUT 1 FOOT ABOVE THE LEVEL OF THE HIGHWAY, KV1684'PENNSYLVANIA DEPARTMENT OF HIGHWAYS DISK DRILLED IN HORIZONTAL. KV1684'STAMPED J 269 1960. KV1684 STATION RECOVERY (2002) KV1684 KV1684 KV1684'RECOVERY NOTE BY US POWER SQUADRON 2002 (ML) KV1684'RECOVERED IN GOOD CONDITION. \*\*\* retrieval complete. Elapsed Time = 00:00:00

#### The NGS Data Sheet

See file \_dsdata.txt for more information about the datasheet.

DATABASE = , PROGRAM = datasheet, VERSION = 7.85 National Geodetic Survey, Retrieval Date = JUNE 30, 2010 1 \*\*\*\*\*\*\* KV1464 DESIGNATION - GATE - KV1464 KV1464 PID KV1464 STATE/COUNTY- PA/NORTHAMPTON KV1464 USGS QUAD - EASTON (1994) KV1464 KV1464 \*CURRENT SURVEY CONTROL KV1464 KV1464\* NAD 83(1986) - 40 41 44. (N) 075 12 35. (W) SCALED KV1464\* NAVD 88 59.580 (meters) (195.47) (feet) ADJUSTED KV1464 GEOID09 KV1464 GEOID HEIGHT--34.06 (meters) COMP KV1464 DYNAMIC HT -59.552 (meters) 195.38 (feet) NAVD 88 KV1464 MODELED GRAV-980,159.1 (mgal) KV1464 KV1464 VERT ORDER - FIRST CLASS II KV1464 KV1464. The horizontal coordinates were scaled from a topographic map and have KV1464.an estimated accuracy of +/- 6 seconds. KV1464 KV1464. The orthometric height was determined by differential leveling and KV1464.adjusted in June 1991. KV1464 WARNING-Repeat measurements at this control monument indicate possible KV1464.vertical movement. KV1464 KV1464.Photographs are available for this station. KV1464 KV1464. The geoid height was determined by GEOID09. KV1464 KV1464. The dynamic height is computed by dividing the NAVD 88 KV1464.geopotential number by the normal gravity value computed on the KV1464, Geodetic Reference System of 1980 (GRS 80) ellipsoid at 45 KV1464.degrees latitude (q = 980.6199 gals.). KV1464 KV1464. The modeled gravity was interpolated from observed gravity values. KV1464 KV1464; North Units Estimated Accuracy East KV1464; SPC PA S -154,340. 814,670. MT (+/- 180 meters Scaled) KV1464 SUPERSEDED SURVEY CONTROL KV1464 KV1464 KV1464 NGVD 29 (??/??/??) 59.794 (m) (f) ADJUSTED 196.17 1 2 KV1464 KV1464.Superseded values are not recommended for survey control. KV1464.NGS no longer adjusts projects to the NAD 27 or NGVD 29 datums. KV1464.See file dsdata.txt to determine how the superseded data were derived. KV1464 KV1464 U.S. NATIONAL GRID SPATIAL ADDRESS: 18TVL822049(NAD 83) KV1464 MARKER: DB = BENCH MARK DISK KV1464 SETTING: 30 = SET IN A LIGHT STRUCTURE KV1464 SP SET: PILLAR

KV1464 STAMPING: 196.217 GATE 1932 KV1464 STABILITY: D = MARK OF QUESTIONABLE OR UNKNOWN STABILITY KV1464 SATELLITE: THE SITE LOCATION WAS REPORTED AS NOT SUITABLE FOR KV1464+SATELLITE: SATELLITE OBSERVATIONS - October 04, 2009 KV1464 KV1464HISTORY- DateCondiKV1464HISTORY- 1932MONUMKV1464HISTORY- 1961GOODKV1464HISTORY- 1978GOODKV1464HISTORY- 1984GOODKV1464HISTORY- 20020105GOODKV1464HISTORY- 20091004GOOD Condition. Report By MONUMENTED CGS CGS NGS USPSQD USPSQD GEOCAC KV1464 KV1464 STATION DESCRIPTION KV1464 KV1464'DESCRIBED BY COAST AND GEODETIC SURVEY 1932 KV1464'AT EASTON. KV1464'AT EASTON, NORTHAMPTON COUNTY, AT THE NORTH END OF NORTH THIRD KV1464'STREET AT ITS JUNCTION WITH COLLEGE AVENUE, AT THE MEMORIAL KV1464'ENTRANCE GATE TO LAFEYETTE COLLEGE, AND IN THE WEST FACE OF THE KV1464'EAST STONE PILLAR. A STANDARD DISK, STAMPED 196.217 GATE 1932 KV1464'AND SET VERTICALLY. KV1464 STATION RECOVERY (1961) KV1464 KV1464 KV1464'RECOVERY NOTE BY COAST AND GEODETIC SURVEY 1961 KV1464'RECOVERED IN GOOD CONDITION. KV1464 KV1464 STATION RECOVERY (1978) KV1464 KV1464'RECOVERY NOTE BY NATIONAL GEODETIC SURVEY 1978 KV1464'RECOVERED IN GOOD CONDITION. KV1464 KV1464 STATION RECOVERY (1984) KV1464 KV1464'RECOVERY NOTE BY US POWER SQUADRON 1984 KV1464'RECOVERED IN GOOD CONDITION. KV1464 KV1464 STATION RECOVERY (2002) KV1464 KV1464'RECOVERY NOTE BY US POWER SQUADRON 2002 (RCN) KV1464'RECOVERED IN GOOD CONDITION. KV1464 KV1464 STATION RECOVERY (2009) KV1464 KV1464'RECOVERY NOTE BY GEOCACHING 2009 (PR) KV1464'DISK HAS ADDITIONAL STAMPING 196.174 \*\*\* retrieval complete. Elapsed Time = 00:00:00

# 12. Appendix F: Control Survey Points

List Points					
Printing					
Point List:	1-12				
🔘 Enable I	Filtering 🛛 🗸 (	Case-sensitive Matchir	Ig		Build List
<ul> <li>List All F</li> <li>Point List</li> </ul>	Points st Entry				Create Group
Raw Desc M	latching Point Group	s Include Exclude	Summary	List	
Number	Northing	Easting	Elevation	Raw Desc	Full Desc
<b>•</b> 1	506266.6114	2672542.8192	180.49	PK-1	PK-1
	506418.5992	2672828.3224	190.74	PK-2	PK-2
4 3	506205.4893	2672117.6822	182.91	PK-3	PK-3
🔶 4	506223.2169	2672548.7359	174.68	PK-4	PK-4
	505814.6982	2671835.5567	186.26	PK-5	PK-5
	506193.0665	2672215.7232	176.96	PK-6	PK-6
🔶 7	505866.2876	2672374.3717	199.36	PK-7	PK-7
4 8	505911.6873	2672870.1154	196.88	PK-8	PK-8
9	505849.5834	2671672.7298	215.12	KV1684	KV1684
<b>�</b> 10	506271.4068	2672580.6067	180.77	PK-64	PK-64
11	506408.6796	2672823.3501	190.31	RRSPK	RRSPK
<b>•</b> 12	506425.8211	2672845.9235	196.22	KV1464	KV1464
Reset		ОК		Cancel	Help

# 13. Appendix G: Complete List of Topographic Points

Raw De	esc Matchir	g Point Groups	Include Exclude	Summary	List	
Numbe	er	Northing	Easting	Elevation	Raw Desc	Full Desc
<b></b>	1	506266.6114	2672542.8192	180.49	PK-1	PK-1
<b></b>	2	506418.5992	2672828.3224	190.74	PK-2	PK-2
<b></b>	3	506205.4893	2672117.6822	182.91	PK-3	PK-3
•	4	506223.2169	2672548.7359	174.68	PK-4	PK-4
	5	505814.6982	2671835.5567	186.26	PK-5	PK-5
	6	506193.0665	2672215.7232	176.96	PK-6	PK-6
<b></b>	7	505866.2876	2672374.3717	199.36	PK-7	PK-7
<b></b>	8	505911.6873	2672870.1154	196.88	PK-8	PK-8
<b></b>	9	505849.5834	2671672.7298	215.12	KV1684	KV1684
<b></b>	10	506271.4068	2672580.6067	180.77	PK-64	PK-64
<b>e</b>	11	506408.6796	2672823.3501	190.31	RRSPK	RRSPK
<b>e</b>	12	506425.8211	2672845.9235	196.22	KV1464	KV1464
<b></b>	14	506134.8690	2672668.5135	181.43	CS1 tb	CS1 tb
<b></b>	15	506139.2528	2672669.4446	176.32	CS1	CS1
¢	16	506145.1111	2672667.7727	169.14	CS1 fp	CS1 fp
•	17	506151.6943	2672668.3666	165.90	CS1 fp	CS1 fp
¢	18	506160.3550	2672668.7246	165.27	CS1 fp	CS1 fp
¢	19	506166.8434	2672669.7441	164.10	CS1 ew	CS1 ew
¢	20	505998.2157	2671966.0837	174.76	hub	hub
¢	21	505998.2157	2671966.0837	174.75	TR	TR
¢	22	506170.1950	2672670.0583	163.25	CS1	CS1
¢	23	506174.8054	2672671.0269	164.16	CS1	CS1
¢	24	506181.4264	2672671.4170	162.89	CS1	CS1
¢	25	506184.8457	2672670.8467	162.29	CS1	CS1
¢	26	506188.9168	2672670.5018	162.19	CS1	CS1
¢	27	506192.2332	2672670.3763	161.95	CS1	CS1
¢	28	506196.6951	2672668.5192	161.92	CS1	CS1
¢	29	506199.6728	2672668.5261	161.84	CS1	CS1
\$	30	506202.9520	2672668.8679	162.59	CS1 eb	CS1 eb
•	31	506206.4044	2672668.9549	163.14	CS1	CS1
•	32	506210.0306	2672668.1757	166.22	CS1	CS1
•	33	506217.8114	2672688.6487	167.85	CS2	CS2
•	34	506214.2840	2672688.2380	167.86	CS2	CS2
•	35	506214.0134	26/2688.2218	168.59	CS2	CS2
*	36	506212.5442	26/2688.2/98	168.54	CS2tw	CS2tw
*	3/	506212.1007	26/268/.6552	164.24	CS2 bw	CS2 bw
*	38	506206.4310	26/268/.3628	164.41	CS2 bw	CS2 bw
Ŷ	39	506206.1396	26/268/./361	168.44	CS2tw	CS2tw
ም ሐ	40	506203.1627	26/2688.2142	101.00	CS2 DW	CS2 DW
ም - እ	41	506201.7766	26/2688.3009	103.00	052	052
Ψ A	42	506199.7017	26/268/.2/60	101.00	052	CS2
Ψ Α	43	500130.3710	26/2686.89/0	102.01	052	CS2
* *	44	500134.3070	2072007.0074	103.03	CS2	CS2
ф ф	46	506190 36/8	2672685 4289	161.03	CS2	CS2
ф ф	47	506187 0680	2672685 5139	167.33	CS2	CS2
ф.	48	506184 0077	2672686 1532	162.23	CS2	CS2
•	49	506180 9812	2672685 8717	162.92	CS2	CS2
•	50	506179 0355	2672686 7702	163.08	CS2 islad	CS2 islad
à	51	506178 1754	2672686 5859	164 70	CS2 islad	CS2 islad
è	52	506171.1089	2672687 9303	165.02	CS2 islad	CS2 islad
÷	53	506166,7555	2672689 4641	161.70	CS2 sb	CS2 sb
•	54	506159.5283	2672687.8708	162.95	CS2 eb	CS2 eb
•	55	506158.3247	2672687.2748	164.27	CS2 tb	CS2 tb
_						

Raw	Desc Ma	tching Point G	iroups Include	Exclude	Summary	List	
Nur	nber	Northir	ng E	asting	Elevation	Raw Desc	Full Desc
¢	56	506155.18	73 267268	6.8637	164.29	CS2 tb	CS2 tb
¢	57	506144.47	57 267268	6.3883	168.04	CS2	CS2
¢	58	506126.88	47 267267	6.5668	187.88	CS2 ts	CS2 ts
¢	59	506268.49	40 267246	0.1489	180.31	CS3 top rd	CS3 top rd
¢	60	506254.21	56 267246	2.7358	180.08	CS3 top banł	CS3 top bank
¢	61	506250.33	87 267246	3.5355	179.46	CS3 top slop	CS3 top slope
¢	62	506243.12	60 267246	5.2258	176.04	CS3 tree	CS3 tree
¢	63	506235.27	35 267246	5.9166	174.28	CS3 mid slop	CS3 mid slope
¢	64	506226.20	48 267246	7.9246	172.31	CS3 bottom s	CS3 bottom slope
¢	65	506220.76	57 267246	7.9553	170.40	CS3 w edge	CS3 w edge
•	66	506266.63	69 267254	2.8157	180.52	bs	bs
•	90	506223.21	69 267254	8.7360	174.68	Start	Start
•	91	506223.21	69 267254	8.7360	174.68	Start	Start
•	92	506193.06	65 267221	5.7232	176.97	Start	Start
	95	506193.13	81 267221	5.5530	177.03	bschk	bschk
•	96	506193.06	65 267221	5.7232	177.04	bschk	bschk
•	97	506266.63	80 267254	2.7973	180.50	bschk	bschk
•	98	506266.63	87 267254	2.7972	180.50	bschk	bschk
•	102	506250.04	39 267257	8.8189	181.09	ER	ER
•	103	506234.44	32 267258	1.0203	172.47	EC	EC
•	104	506223.80	29 26/258	1.3837	1/2.26	EC	EC
•	105	506289.17	28 26/25/	6.6809	180.69	ER	ER
•	106	506220.88	47 267258	2.1865	168.92	EC	EC
•	107	506219.77	54 267258	0.3755	161.85	EB	EB
•	108	506216.09	/8 26/258	1.3848	161.05	CHAN	CHAN
•	109	506210.59	01 26/258	2.2486	161.05	CHAN	CHAN
•	110	506209.78	19 26/258	2.5048	160.78	CHAN	CHAN
*	111	506204.71	58 26/258	2.7820	160.66	CHAN	CHAN
*	112	506204.03	44 26/258	2.7436	161.00	CHAN	CHAN
₩ A	113	506198.09	26/238	3.53/8	101.01	CHAN	CHAN
~	114	506152.06	00 207250	3.0456	100.37		CHAN
*	110	500103.13	20 207230	4.3303	100.70		CD
*	117	500102.74	04 207230	4.3033	101.70		CD
*	110	506160.23	20 207250	9.0465	160.76	CD	CD
Å	110	506150.30	34 207257 AD 267255	7 9105	160.70	CD	CD
ф (ф	120	506213 32	62 267255	4 6908	161 37	Slope 6' fr wa	Slope 6' fr wall
ф.	121	506213.32	57 267259	4 0062	159.66	SP	SP
ф.	122	506207.11	09 267259	4 5814	159 12	FP	FP
<b>\$</b>	123	506196.88	81 267259	4 8867	158.62	FP	FP
*	124	506188 78	92 267258	5 1359	158.84	FP	FP
å	125	506187.80	89 267258	5 3263	158.45	FP	FP
ф (ф	125	506183.59	93 267258	5 2540	158.56	EP	EP
\$	127	506180.44	56 267258	5 7320	158.18	FP	FP
<b>\$</b>	128	506176.65	36 267258	5 7970	158.82	FP	FP
\$	129	506173.59	25 267258	6 0297	159.99	FP	FP
è	130	506170.07	29 267258	5 9582	160.45	EP	EP
è	131	506165 15	15 267258	6.2671	160.47	EP	EP
¢	132	506159.63	91 267258	3.8397	173.65	PIPE INV	PIPE INV
¢	133	506157.82	92 267258	4.0672	181.89	CNC	CNC
•	134	506156 19	68 267258	3.9377	181.94	CNC	CNC
¢	135	506156 19	85 267258	4.0114	181.94	CNC	CNC
¢	136	506156.04	35 267258	4.1450	179.42	CNC	CNC
¢	137	506150 23	31 267257	4.4762	179.80	UP	UP
- <b>-</b>		000100.20					

Raw	Desc Mat	ching	Point Group	ps Include	e Exclude	Summary	List		
Nur	nber		Northing		Easting	Elevation	Raw D	esc	Full Desc
•	138	50	6117,4794	26725	576.5124	180.53	СВ		CB
•	139	50	6115.8063	26725	544.6029	181.02	CB		СВ
•	140	50	6137.9065	26725	543.3488	180.75	СВ		CB
\$	141	50	6136.6544	26725	515.2557	180.78	СВ		СВ
•	142	50	6157.1625	26725	574.3539	181.69	cw		cw
•	143	50	6155.4125	26725	574.5760	179.72	cw		cw
•	144	50	6186.6306	26726	80.4562	163.80	cbp		cbp
\$	145	50	6187.4585	26726	98.5664	164.67	cbp		cbp
\$	146	50	6188.2437	26727	715.2037	163.44	cbp		cbp
•	147	50	6188.8666	26727	731.8529	163.48	cbp		cbp
•	148	50	6189.5691	26727	744.5092	163.64	cbp		cbp
•	149	50	6186.7323	26728	37.6202	159.62	3 brg		3 brg
•	150	50	6178.9292	26728	338.3168	159.52	3 brg		3 bra
•	151	50	6291.2145	26725	593.0293	180.75	cross 1		cross 1
•	152	50	6251.3843	26725	595.2933	181.02	cross 1		cross 1
•	153	50	6251.3291	26725	595.3269	181.02	cross 1		cross 1
•	154	50	6234.5297	26725	594.5327	171.78	cross 1		cross 1
•	155	50	6225.4980	26725	594.2806	171.50	cross 1		cross 1
•	156	50	6224.9724	26725	594.6530	164.47	cross 1		cross 1
•	157	50	6217.5445	26725	594.7442	164.07	cross 1		cross 1
•	158	50	6217.0353	26725	594.6946	158.69	cross 1		cross 1
¢	159	50	6217.0353	26725	594.6946	158.69	cross 1		cross 1
¢	160	50	6213.9634	26725	594.8380	157.96	cross 1		cross 1
•	161	50	6207.3310	26725	595.8170	156.20	cross 1		cross 1
•	162	50	6199.9157	26725	598.5145	156.02	cross 1		cross 1
¢	163	50	6192.1722	26725	597.9903	157.68	cross 1		cross 1
¢	164	50	6186.9182	26725	598.2069	158.52	cross 1		cross 1
•	165	50	6181.9258	26725	598.5805	159.16	cross 1		cross 1
¢	166	50	6176.1533	26725	599.6674	161.93	cross 1		cross 1
¢	167	50	6171.2219	26725	599.7185	162.47	cross 1		cross 1
•	168	50	6171.0722	26725	599.5957	164.96	cross 1		cross 1
•	169	50	6165.9952	26726	500.2094	167.85	cross 1		cross 1
¢	170	50	6159.6943	26726	501.2201	169.51	cross 1		cross 1
¢	171	50	6152.3919	26726	602.6479	168.67	cross 1		cross 1
•	172	50	6145.6319	26726	517.4727	170.81	cross 2		cross 2
•	173	50	6173.2490	26726	517.1768	157.57	cross 2		cross 2
¢	174	50	6174.2120	26726	517.3835	158.33	cross 2		cross 2
•	175	50	6179.9715	26726	516.6046	157.22	cross 2		cross 2
•	176	50	6185.8515	26726	517.8674	156.34	cross 2		cross 2
•	177	50	6190.3569	26726	517.1557	159.44	cross 2		cross 2
•	178	50	6195.6257	26726	518.8922	158.32	cross 2		cross 2
•	179	50	6200.9095	26726	519.9035	158.28	cross 2		cross 2
•	180	50	6207.4416	26726	519.2896	158.93	cross 2		cross 2
•	181	50	6214.0985	26726	517.9764	160.37	cross 2		cross 2
•	182	50	6217.5170	26726	517.9500	160.87	cross 2		cross 2
•	183	50	6217.6014	26720	517.9720	163.25	cross 2		cross 2
•	184	50	6221.5746	26726	517.1173	163.49	cross 2		cross 2
₩ ~	185	50	6221.6774	26720	17.2626	166.08	cross 2		cross 2
₩ •	186	50	6230./369	26/26	517.9057	165.82	cross 2		cross 2
<b>*</b>	187	50	6231.0307	26/26	018.012/	1/0.6/	cross 2		cross 2
<b>*</b>	188	50	0236.4/20	26/26	016.8445	1/0.49	cross 2		cross 2
₩ ▲	100	50	0203.3/65	26/20	211.2542	101.00	cross 2		cross 2
₩ ▲	101	50	0237.2100	20/20	511.3043	170.00	cross 2		cross 2
	191	50	6150.8318	26/26	007.9060	176.06	cross 3		CIOSS 3

Raw	Desc Mate	ching Point Groups	Include Exclude	Summary	List	
Nun	nber	Northing	Easting	Elevation	Raw Desc	Full Desc
¢	192	506164.4684	2672655.1611	167.34	cross 3	cross 3
¢	193	506176.0624	2672652.9790	166.13	cross 3	cross 3
¢	194	506176.7591	2672652.3403	162.71	cross 3	cross 3
ф	195	506185.2609	2672651.7617	161.66	cross 3	cross 3
ф	196	506194.3915	2672651.1657	161.80	cross 3	cross 3
¢	197	506202.2043	2672651.4604	162.04	cross 3	cross 3
¢	198	506208.2140	2672651.4098	162.91	cross 3	cross 3
¢	199	506213.6642	2672650.5142	163.62	cross 3	cross 3
¢	200	506221.4688	2672650.3530	164.25	cross 3	cross 3
¢	201	506229.5099	2672652.1853	170.52	cross 3	cross 3
¢	202	506252.8802	2672648.1569	182.33	cross 3	cross 3
¢	302	506279.7035	2672531.0961	180.79	CS 1 rd	CS 1 rd
¢	303	506265.1634	2672534.9652	180.52	CS 1 rd	CS 1 rd
¢	304	506248.5785	2672539.7060	180.52	CS 1	CS 1
¢	305	506236.4105	2672541.4089	174.86	CS 1	CS 1
¢	306	506219.0635	2672545.0629	174.79	CS 1	CS 1
¢	307	506218.4761	2672545.1878	169.74	CS 1 dam	CS 1 dam
¢	308	506276.9545	2672522.1776	180.72	CS 2	CS 2
¢	309	506262.7586	2672527.1588	180.50	CS 2	CS 2
¢	310	506251.1487	2672528.4860	180.10	CS 2	CS 2
¢	311	506228.4434	2672536.1615	170.40	CS 2	CS 2
¢	312	506159.7100	2672557.9878	169.80	CS 1 dam	CS 1 dam
¢	313	506221.8761	2672535.1386	168.69	CS 2	CS 2
¢	314	506216.3956	2672536.9408	167.15	CS 2	CS 2
¢	315	506164.9342	2672549.1680	167.07	CS 2	CS 2
¢	316	506158.3214	2672550.3721	169.57	CS 2	CS 2
¢	317	506159.3424	2672558.1663	174.68	CS 1 cnc	CS 1 cnc
¢	318	506155.9081	2672550.0672	174.44	CS 2 cnc	CS 2 cnc
¢	319	506216.6874	2672533.9732	166.35	CS 3	CS 3
¢	320	506210.6274	2672536.1189	166.05	CS 3	CS 3
¢	321	506203.7130	2672537.4109	166.34	CS 3	CS 3
¢	322	506195.8435	2672539.9509	166.37	CS 3	CS 3
¢	323	506190.2218	2672541.0070	166.54	CS 3	CS 3
¢	324	506183.1059	2672543.1253	166.50	CS 3	CS 3
•	325	506177.8016	2672543.6595	166.60	CS 3	CS 3
•	326	506170.6476	2672545.1289	166.46	CS 3	CS 3
•	327	506165.6515	2672546.1189	166.60	CS 3	CS 3
•	328	506163.4913	2672547.2196	168.21	CS 3	CS 3
¢	329	506158.1533	2672549.4328	169.82	CS 3 eb	CS 3 eb
•	330	506155.5669	2672549.0407	174.60	CS 3 cnc	CS 3 cnc
¢	331	506267.9774	2672492.6075	180.45	CS 4	CS 4
•	332	506253.3247	2672496.1860	180.43	CS 4	CS 4
¢	333	506243.2842	2672498.5966	178.95	CS 4	CS 4
•	334	506237.2177	2672499.7805	174.99	CS 4	CS 4
•	335	506219.4502	2672506.9518	167.28	CS 4	CS 4
\$	336	506212.4560	2672509.6534	165.12	CS 4	CS 4
\$	337	506203.7146	2672510.3221	166.31	CS 4	CS 4
•	338	506196.7255	2672510.7964	166.52	CS 4	CS 4
<b>\$</b>	339	506187.7782	2672510.3796	166.33	CS 4	CS 4
<b>*</b>	340	506180.3330	2672510.3144	166.18	CS 4	CS 4
<b>\$</b>	341	506172.8598	2672511.3011	165.78	CS 4	CS 4
•	342	506167.2672	26/2511.1409	165.60	CS 4	CS 4
<b>\$</b>	343	506158.4522	2672511.8901	170.71	CS 4	CS 4
¢	344	506154.1996	2672515.0322	177.65	CS 4	CS 4

Raw	Desc Mat	ching Point Gr	oups Include	Exclude	Summary	List		
Nur	nber	Northing	, Е	asting	Elevation	Raw De	sc	Full Desc
¢	345	506254.832	9 267249	8.7089	179.99	tele		tele
•	346	506270.416	2 267246	1.5144	180.25	CS 5		CS 5
•	347	506255.706	0 267246	3.9591	180.05	CS 5		CS 5
¢	348	506250.349	1 267246	5.6855	178.89	CS 5		CS 5
¢	349	506237.568	7 267246	6.4708	174.37	CS 5		CS 5
¢	350	506221.634	7 267246	6.9318	170.46	CS 5		CS 5
•	351	506220.043	0 267246	7.0361	169.12	CS 5		CS 5
•	352	506219.292	9 267246	7.0347	165.25	CS 5		CS 5
•	353	506211.887	4 267246	8.0628	165.23	CS 5		CS 5
•	354	506203.249	2 267246	8.2660	166.17	CS 5		CS 5
•	355	506198.370	3 267246	8.2196	166.25	CS 5		CS 5
¢	356	506189.674	5 267246	7.9780	166.77	CS 5		CS 5
¢	357	506183.250	6 267246	7.8545	166.99	CS 5		CS 5
•	358	506174.445	1 267246	7.4894	167.25	CS 5		CS 5
•	359	506165.287	2 267246	8.2328	166.91	CS 5		CS 5
•	360	506157.335	9 267246	8.7599	167.00	CS 5		CS 5
•	361	506151.451	1 267246	9.1322	170.09	CS 5		CS 5
•	362	506146.126	5 267246	9.5037	174.65	CS 5		CS 5
•	363	506137.572	0 267246	7.7292	179.60	CS 5		CS 5
•	364	506261.160	3 267240	3.9644	179.81	CS 6		CS 6
•	365	506245.871	7 267240	6.6842	179.68	CS 6		CS 6
•	366	506225.108	4 267241	0.9349	172.82	CS 6		CS 6
•	367	506218.858	4 26/241	1.5092	1/1.4/	CS 6		CS 6
•	368	506217.820	6 26/241	1.5434	1/0.39	CS 6		CS 6
•	369	506216.238	3 26/241	1.6855	1/0.24	CS 6		CS 6
*	3/0	506215.999	8 26/241	1.5219	168.82	CS 6		CS 6
₩ ~	3/1	506212.684	0 26/241	1.8393	168.03	CS 6		0.00
₩ A	372	506210.610	9 26/241	1.0381	107.06	CSG		0.0
A A	3/3	506203.673	0 20/241	3.9010	104.77	000		C5 6
Å	374	500130.700	0 267241	3.7004	160.00	C3 6		C36
Å	276	506132.037	207241	4.4374 6.2274	165.70	0 6 2		C36
Å	370	506176 669	0 267241	6 7/82	165.70	0.60		0.00
<b>Å</b>	378	506169.831	5 267241	6 9963	166.47	0.00		0.00
à	379	506166.262	5 267241	6.8750	166 10	0.00		CS 6
å	380	506161.841	6 267241	5 9566	166.32	CS 6		CS 6
۵.	381	506158 100	0 267241	5 2659	167.46	CS 6		CS 6
•	382	506153.702	7 267241	4.3410	170.19	CS 6		CS 6
•	383	506151.993	4 267241	4.4214	172.26	CS 6		CS 6
•	384	506139.080	4 267241	2.5797	184.34	CS 6		CS 6
•	403	506247.635	9 267234	2.2496	180.28	cs1 rd		cs1 rd
•	404	506234.392	7 267234	4.6367	179.74	cs1 rd		cs1 rd
•	405	506199.807	3 267234	9.5841	170.04	cs1		cs1
•	406	506199.182	9 267235	0.0141	166.61	cs1		cs1
•	407	506193.952	6 267235	0.8000	164.73	cs1		cs1
•	408	506187.817	4 267235	3.3695	164.28	cs1		cs1
•	409	506177.800	8 267235	2.1362	164.96	cs1		cs1
•	410	506172.395	7 267235	2.2146	165.41	cs1 log		cs1 log
•	411	506169.798	3 267235	0.8730	166.82	cs1 log		cs1 log
•	412	506165.742	9 267235	2.8205	165.48	cs1		cs1
•	413	506158.256	7 267235	3.9891	164.82	cs1		cs1
•	414	506151.965	0 267235	5.7826	165.99	cs1		cs1
•	415	506149.879	2 267235	5.6301	169.32	cs11		cs11
¢	416	506147.045	6 267235	5.9325	169.31	cs1		cs1

Raw	Desc Mat	ching Point Groups	Include Exclude	Summary	List		
Nur	nber	Northing	Easting	Elevation	Raw Desc	Full Desc	
¢	417	506128.5697	2672356.9363	185.30	cs1	cs1	
¢	418	506121.4430	2672357.6641	185.21	cs1 bldg	cs1 bldg	
¢	419	506116.8309	2672299.5278	186.55	wall	wall	
¢	420	506128.4254	2672298.2973	186.12	wall	wall	
¢	421	506128.4017	2672297.5932	176.35	wall	wall	
¢	422	506131.8036	2672297.2419	173.61	cs2	cs2	
¢	423	506135.5718	2672297.0997	171.41	cs2	cs2	
¢	424	506136.0855	2672297.1324	170.29	cs2	cs2	
¢	425	506139.3229	2672296.1714	168.75	cs2	cs2	
¢	426	506143.5546	2672295.4034	166.68	cs2	cs2	
¢	427	506150.9936	2672294.8582	166.17	cs2	cs2	
¢	428	506158.0348	2672294.0661	165.58	cs2	cs2	
¢	429	506164.8452	2672295.3233	165.45	cs2	cs2	
¢	430	506172.4189	2672294.4161	165.13	cs2	cs2	
¢	431	506180.1086	2672294.5956	164.45	cs2	cs2	
¢	432	506186.6058	2672292.4736	164.72	cs2	cs2	
¢	433	506192.1542	2672292.6203	165.13	cs2	cs2	
¢	434	506192.7625	2672292.4708	165.23	cs2	cs2	
¢	435	506193.3538	2672292.3827	171.04	cs2	cs2	
¢	436	506197.7369	2672290.4893	171.41	cs2	cs2	
¢	437	506217.4110	2672289.3783	178.81	cs2	cs2	
¢	438	506223.8552	2672288.2538	179.78	cs2 rd	cs2 rd	
¢	439	506239.4478	2672284.7544	180.54	cs2 rd	cs2 rd	
¢	440	506232.3623	2672217.0510	181.28	cs3 rd	cs3 rd	
¢	441	506216.9260	2672220.1329	180.60	cs3 rd	cs3 rd	
¢	442	506201.8664	2672223.3255	178.24	cs3	cs3	
¢	443	506184.8756	2672223.5843	170.18	cs3	cs3	
¢	444	506184.0174	2672224.4570	167.24	cs3	cs3	
¢	445	506181.2693	2672224.6573	165.74	cs3	cs3	
•	446	506177.2626	2672226.5599	164.49	cs3	cs3	
•	447	506171.4201	2672224.8290	164.07	cs3	cs3	
•	448	506164.7630	2672226.6112	164.90	cs3	cs3	
•	449	506156.0333	2672228.4653	165.95	cs3	cs3	
<b>*</b>	451	506147.6036	2672229.7366	167.43	cs3	cs3	
÷	452	506138.3302	26/2230.0682	168.66	cs3	cs3	
¢	453	506126.9245	2672231.9362	169.14	cs3	cs3	
<b>*</b>	454	506125.5182	2672233.5695	1/2.13	cs3	cs3	
*	455	506121./388	26/2233.3999	1/8.04	cs3	cs3	
<b>*</b>	456	506107.3877	2672235.5794	188.26	cs3	cs3	
*	457	506102.4454	26/2236.1908	188.29	cs3	cs3	
<b>•</b>	458	506122.6187	26/2186.9951	169./1	cnc wall	cnc wall	
*	459	506126.2642	26/2213.9311	168.80	cnc wall	cnc wall	
*	460	506127.1529	26/2214.0/65	167.54	cnc wall	cnc wall	
<b>*</b>	461	506122.8138	26/2186./384	168.60	cnc wall	cnc wall	
<b>*</b>	462	506120.4663	26/2186./925	1/0.01	cnc wall	cnc wall	
*	463	506120.4219	26/2186.4/24	169.28	cnc wall	cnc wall	
<b>*</b>	464	506090.1787	2672176.8497	188.44	cs4	cs4	
*	465	506090.5381	26/21/6.6329	186.65	cs4	cs4	
*	466	506107.8466	26/2165.5098	1/1.38	cs4	cs4	
* *	467	506108.3021	26/2165.3203	169.89	cs4	cs4	
*	468	506112./183	26/2162.5043	169.39	CS4	CS4	
* *	469	506125.8995	26/2156.7374	168.28	cs4	cs4	
* ~	4/0	506137.5171	26/2151.4461	167.23	cs4	cs4	
÷	471	506141.0847	2672149.3441	168.59	cs4	cs4	

Rav	v Desc Mat	ching Point Groups	Include Exclude	Summary	List	
Nu	mber	Northing	Easting	Elevation	Raw Desc	Full Desc
	472	506146.5681	2672146.3215	168.15	cs4	cs4
•	473	506147.4456	2672144.5345	166.54	cs4	cs4
•	474	506155.9641	2672140.2269	165.07	cs4	cs4
•	475	506160.2544	2672138.0070	165.14	cs4	cs4
•	476	506164.6341	2672136.5300	166.36	cs4	cs4
•	477	506167.7253	2672135.4638	169.06	cs4	cs4
•	478	506170.0832	2672134.4160	170.22	cs4	cs4
•	479	506170.6250	2672134.7226	171.35	cs4	cs4
•	480	506184.9455	2672129.7358	182.71	cs4	cs4
\$	481	506193.3235	2672126.9476	182.61	cs4 rd	cs4 rd
¢	482	506205.7521	2672122.5520	182.67	cs4 rd	cs4 rd
	483	506180.2749	2672204.0375	167.33	wood strctr	wood strctr
•	484	506179.7872	2672204.3026	166.05	wood strctr	wood strctr
•	485	506173.6134	2672194.8780	166.38	wood strctr	wood strctr
¢	486	506169.6084	2672189.0182	166.39	wood strctr	wood strctr
¢	487	506181.6105	2672193.5837	166.95	wood strctr	wood strctr
•	488	506163.2020	2672179.6332	166.39	wood strctr	wood strctr
•	489	506163.2694	2672180.0416	166.02	wood strctr	wood strctr
•	490	506165.5886	2672183.3551	165.87	wood strctr	wood strctr
•	491	506169.7339	2672189.6711	165.56	wood strctr	wood strctr
•	492	506177.3929	2672201.3928	165.14	wood strctr	wood strctr
•	493	506174.4748	2672197.2174	165.10	wood strctr	wood strctr
•	494	506173.0656	2672194.1804	164.90	wood strctr	wood strctr
¢	495	506179.2278	2672187.1523	166.46	wood strctr	wood strctr
•	496	506170.9108	2672174.8976	166.14	wood strctr	wood strctr
•	497	506171.0729	2672174.9136	165.77	wood strctr	wood strctr
•	498	506170.2968	2672175.6720	166.25	wood strctr	wood strctr
•	499	506170.2383	2672175.8216	165.83	wood strctr	wood strctr
¢	500	506136.0513	2672141.3434	167.38	rocks	rocks
•	501	506137.3094	2672142.9005	168.48	rocks	rocks
•	502	506139.7482	2672141.1672	167.26	rocks	rocks
•	503	506138.0033	2672145.1665	167.43	rocks	rocks
•	504	506143.9083	26/2141.4282	167.26	rocks	rocks
•	505	506139.2836	26/2146.5828	168.47	rocks	rocks
•	506	506143.4257	26/2142.03/5	167.80	rocks	rocks
*	507	506139.5717	26/2149./234	167.54	rocks	rocks
<b>*</b>	508	506147.3164	26/2144.8635	166.57	rocks	rocks
₩ ▲	510	500140.3685	20/2149.3922	100.3/	rocks	rocks
₩ ▲	510	506140.2010	2072140.0009	100.00	rocks	moke
*	512	506140.0073	2672103.0047	107.43	moke	moke
* *	512	5061/0.2057	2672143.1010	160.00	moke	moke
<b>↓</b>	51/	5061/19 /1972	2672133.3270	167.70	moke	moke
<b>\$</b>	515	506142 1292	2672158 7797	166.99	meks	moks
•	516	506148 5309	2672152 6535	167 15	rocks	rocks
۵.	517	506142 2920	2672158 8396	167.92	rocks	rocks
¢.	518	506147 2801	2672153 3627	167.86	rocks	rocks
•	519	506144,9855	2672162.8200	166.50	rocks	rocks
•	520	506149.3682	2672158.3771	167.29	rocks	rocks
•	521	506145.1179	2672162.6201	167.62	rocks	rocks
•	522	506148.3037	2672159.0424	168.54	rocks	rocks
•	523	506144.2904	2672164.9747	166.47	rocks	rocks
•	524	506150.6770	2672160.9588	167.56	rocks	rocks
•	525	506144.4475	2672164.7316	168.39	rocks	rocks

Raw	Desc Matchi	ing Point Groups	Include Exclude	Summary	List	
Nur	nber	Northing	Easting	Elevation	Raw Desc	Full Desc
¢	526	506151.5048	2672161.4679	166.78	rocks	rocks
¢	527	506145.3017	2672166.0897	166.83	rocks	rocks
¢	528	506151.9084	2672162.7277	166.68	rocks	rocks
¢	529	506145.7393	2672166.2067	168.33	rocks	rocks
¢	530	506149.8484	2672167.1868	167.19	rocks	rocks
¢	531	506147.0839	2672168.5221	166.83	rocks	rocks
¢	532	506149.3795	2672167.4411	168.03	rocks	rocks
¢	533	506148.0987	2672168.7118	168.09	rocks	rocks
¢	534	506150.1915	2672170.7929	167.64	rocks	rocks
¢	535	506150.6110	2672172.0876	166.47	rocks	rocks
¢	536	506147.2780	2672164.2877	168.10	rocks	rocks
¢	537	506147.6793	2672159.4396	168.37	rocks	rocks
¢	538	506145.2022	2672164.8360	168.40	rocks	rocks
¢	539	506147.5180	2672156.6116	168.44	rocks	rocks
¢	540	506146.3485	2672160.2972	168.26	rocks	rocks
•	541	506144.6822	2672157.0851	168.54	rocks	rocks
\$	542	506147.2955	2672154.8529	168.00	rocks	rocks
•	543	506143.4794	2672156.0706	167.93	rocks	rocks
•	544	506145.5214	2672152.5638	168.49	rocks	rocks
•	545	506142.5518	2672152.5563	168.60	rocks	rocks
•	546	506146.8757	2672148.4962	167.36	rocks	rocks
•	547	506142.1351	2672148.1676	168.55	rocks	rocks
•	548	506148.4830	2672146.4901	167.81	rocks	rocks
•	549	506143.6873	2672146.4200	168.86	rocks	rocks
•	550	506146.7506	2672145.5206	167.31	rocks	rocks
•	551	506142.1603	2672145.5052	168.38	rocks	rocks
•	552	506146.2702	2672145.1986	168.90	rocks	rocks
•	553	506139.6534	26/2145.2533	168.86	rocks	rocks
•	554	506143.8788	26/2145.1/63	168.04	rocks	rocks
*	555	506139.4757	26/2144.442/	168.14	rocks	rocks
₩ ~	555	506141.4529	26/2141.8/65	168.76	rocks	rocks
₩ ▲	550	506138.4995	26/2142.5922	107.55	rocks	rocks
*	500	506137.8836	26/2140.3200	167.00	rocks	rocks
*	000	500120.1132	20/2120.1344	100.30	TOCKS	rocks
*	500	506122.5565	20/2112.00/4	103.20	rocks	rocks
*	501	506123.0200	20/2120.00/0	100.30	rocks	rocks
	562	506122.7003	2672112.4031	169.00	moke	moke
*	564	506127 0268	2672111 8817	169.09	moks	moks
*	565	506130 2424	2672117 7215	168.05	meks	moks
<b>\$</b>	566	506126 8894	2672111 4928	168.22	rocks	rocks
<b>\$</b>	567	506128 7035	2672119 5617	168.41	rocks	rocks
*	568	506124 6456	2672110.8080	168.91	meks	moks
*	569	506124 7782	2672110.8002	168.91	meks	moks
<b>\$</b>	570	506075 8574	2672115 5857	169.91	cs5	cs5
\$	571	506083 9882	2672110 9461	168.86	cs5	cs5
•	572	506090 9776	2672106 2866	168.67	cs5	cs5
å	573	506097 3927	2672101 9927	168.86	cs5	cs5
å	574	506103 0856	2672098 5730	169.82	cs5	cs5
÷	575	506108.3464	2672095 4367	169.18	cs5	cs5
÷	576	506115 1237	2672092 5396	170.31	cs5	cs5
•	577	506124 1031	2672089 9949	168.93	cs5	cs5
÷	578	506132,7340	2672086.9807	168 29	cs5	cs5
•	579	506143 6391	2672082 0100	167.05	cs5	cs5
			20.2002.0100			

Raw	Desc Mat	ching F	oint Group	s Include	Exclude	Summary	List		
Nur	nber		Northing	E	Easting	Elevation	Raw De	sc	Full Desc
\$	580	506	150.1570	267207	8.8640	166.83	cs5		cs5
•	581	506	155.6795	267207	8.3742	169.49	cs5		cs5
•	582	506	177.6595	267207	3.6945	183.70	cs5		cs5
¢	583	506	187.7810	267206	9.1136	183.69	cs5		cs5
•	600	506	187.4301	267205	8.0599	183.98	eopk		eopk
•	601	506	175.1893	267206	2.2414	183.36	eop		eop
•	602	506	175.1413	267206	2.3320	183.84	eop		eop
•	603	506	175.8641	267206	6.7823	183.28	tb		tb
•	604	506	160.1870	267206	9.5713	171.49	bb		bb
•	605	506	150.7106	267207	1.2142	166.92	left Ban	k	left Bank
•	606	506	140.5752	267207	3.3127	167.73	bc		bc
•	607	506	118.9012	267207	9.3676	170.09	bc		bc
•	608	506	109.0755	267208	2.6472	170.09	left Ban	k	left Bank
•	609	506	102.3306	267208	5.5228	169.46	bc		bc
•	610	5060	088.7745	267209	4.1186	168.66	bc		bc
•	611	5060	073.2199	267210	4.7961	169.65	right Ba	nk	right Bank
•	612	5060	059.5290	267211	2.2435	174.07	bb		bb
•	613	5060	36.7563	267212	2.9990	188.65	tb		tb
•	614	5060	010.4320	267209	0.7182	187.69	tb		tb
¢	615	506	168.7736	267199	6.1722	184.22	bp		bp
¢	616	506	155.4720	267200	0.5365	183.92	fp		fp
¢	617	506	151.1249	267200	2.6466	183.58	tb		tb
•	618	5060	024.3140	267208	2.3029	176.88	bb		bb
•	619	506	134.8925	267200	7.2600	170.36	bb		bb
•	620	5060	44.2227	267207	4.7357	170.14	bb		bb
•	621	506	129.1250	267200	7.1828	167.55	left Ban	k	left Bank
•	622	5060	060.1981	267206	1.0104	169.04	bc		bc
¢	623	5061	124.7187	267200	7.7485	166.76	bc		bc
•	624	5060	071.5302	267205	0.5521	170.12	bc		bc
•	625	506	120.2966	267200	9.0200	167.33	bc		bc
¢	626	5060	082.3719	267203	2.9393	173.72	is		is
¢	627	5061	110.4077	267201	4.6025	168.45	bc		bc
•	628	5060	099.4579	267202	0.5666	170.19	right Ba	nk	right Bank
¢	629	5060	081.8368	267199	7.9375	170.34	right Ba	nk	right Bank
•	630	506	107.3190	267197	2.7154	167.35	left Ban	k	left Bank
•	631	5060	074.2269	267200	3.8330	171.24	right Ba	nk	right Bank
¢	632	506	113.3295	267196	8.8395	170.04	left Ban	k	left Bank
•	633	5060	065.2088	267201	0.6814	173.43	is		is
•	634	506	119.1035	267196	6.3340	175.25	bb		bb
•	635	5060	46.4121	267203	0.0437	169.66	left Ban	k	left Bank
•	636	506	29.9459	267196	1.5616	182.62	tb		tb
•	637	5060	39.0763	267203	6.6601	169.33	bc		bc
•	638	506	132.9354	267196	0.4648	182.95	tp		tp
•	639	5060	025.2246	267204	7.3698	170.22	πρ I		rp I
•	640	506	146.6225	267195	2.8548	183.19	bp		bp
₩ •	641	5060	011.6103	267205	7.6107	1/7.35	bb		DD
₩ •	642	506	103.0113	267197	7.9964	167.56	bc		DC
<b>•</b>	643	5060	194.6195	26/198	5.7908	168.63	DC		DC
₩ •	644	5055	392.6510	26/206	0.2988	189.60	(D)	-1-	ID sinkt Dank
₩ ▲	645	5060	J49.4831	267198	0.4815	1/0.46	ngnt Ba	nĸ	ngnt Bank
₩ ▲	645	5000	7/1.0692	26/205	0.3240	100.15	(D		lD ha
₩ ▲	64/	5050	302.000	26/196	0.2331	172.01	DC	ola	right Paper
₩ ▲	04ŏ	5000	000000000000000000000000000000000000000	20/202	0.21/1	1/2.01	ngnt Ba	IK	hght bank
1 <b>P</b>	649	2060	07.8483	267195	0000.00	169.07	DC		DC

Num	iber	Northing	Easting	Elevation	Raw Desc	Full Desc
\$	650	506076.5652	2671948.4597	168.92	bc	bc
•	651	505993.3219	2672021.1539	170.34	right Bank	right Bank
•	652	506080.9020	2671938.8433	168.56	bc	bc
•	653	506001.9776	2672011.9263	170.17	bc	bc
¢	654	506084.2897	2671934.4488	170.95	left Bank	left Bank
•	655	506005.7308	2672002.3607	169.21	left Bank	left Bank
¢	656	506091.5025	2671927.0090	173.76	bb	bb
•	657	506011.7561	2671990.6561	174.01	is	is
¢	658	506020.5246	2671977.7110	173.93	is	is
¢	659	506101.3450	2671919.2010	181.72	tb	tb
¢	660	506103.8496	2671917.3188	182.09	fb	fb
¢	661	506117.2236	2671908.9775	182.74	bp	bp
¢	662	506031.7389	2671967.5184	170.20	right Bank	right Bank
¢	663	506074.6806	2671863.4381	182.07	right Bank	right Bank
¢	664	506074.6853	2671863.4890	182.04	еор	еор
•	665	506064.7531	2671875.8229	181.26	еор	еор
•	666	506058.5354	2671884.1078	180.87	tb	tb
•	667	506007.2855	2671949.7098	170.65	eow	eow
•	668	506050.3314	2671897.9071	172.55	bb	bb
•	669	505999.9454	2671962.2004	174.19	isl	isl
•	670	506043.4392	2671906.2678	170.24	eow	eow
•	671	505994.5796	2671968.5035	174.07	isl	isl
•	672	506034.2331	2671919.6515	169.54	bc	bc
•	673	505985.2638	2671980.7976	171.05	bc	bc
•	674	506022.6728	26/1931.5905	169.07	bc	bc
•	6/5	5059/5.833/	26/1992.99/4	1/0.03	bc	bc
*	6/6	506013.5562	26/1941./411	158.93	bC	bc
₩ •	6//	505969.6320	26/1998.5146	170.45	DC	DC
~	6/8	506007.1194	2671949.8989	170.63	DC	DC
*	6/3	505050.3007	2672006.1730	170.05	DD	DD
*	C01	505970.3004	2671920.7022	1/0.33	bo	bo
	692	505945 6066	2672019.0707	192./2	elone	elone
- -	683	505979 3484	2671909.0600	168.94	he	ho
<u>م</u>	684	505983 4785	2671901 5691	169.84	bo	bc
	685	505991 3020	2671891 3304	170.36	bo	bc
å	686	505934 3772	2672026 9639	196.05	th	th
•	687	505996.3282	2671884.5269	170.95	eow	eow
•	688	505949.5337	2672028.9122	187.51	tw	tw
•	689	506001.1902	2671877.0350	174.08	bb	bb
•	690	505922.7712	2671981.6629	198.18	tw	tw
•	691	506010.2353	2671863.1075	177.51	tb	tb
¢	692	505949.9812	2672028.5752	186.01	bw	bw
	693	506010.0263	2671853.1457	181.01	slp	slp
	694	505937.4684	2672005.5830	178.05	bw	bw
	695	506011.9040	2671841.4437	181.45	еор	еор
\$	696	505924.0384	2671981.5607	174.43	bw	bw
\$	697	506015.4474	2671825.8676	182.03	еор	еор
¢	698	505931.8808	2671980.7639	173.45	bb	bb
¢	699	505935.2984	2671974.2950	170.58	eow	eow
¢	700	505936.7643	2671970.7981	170.25	bc	bc
¢	701	505972.6977	2671804.4008	183.39	еор	еор
\$	702	505967.5545	2671817.9642	183.39	еор	еор
¢	703	505939.3607	2671967.1133	169.85	bc	bc

Raw	Desc Match	ning Point Groups	Include Exclude	Summary	List	
Nun	nber	Northing	Easting	Elevation	Raw Desc	Full Desc
¢	704	505960.2206	2671841.5002	182.26	еор	еор
¢	705	505941.2612	2671961.1629	172.31	isl	isl
¢	706	505958.7608	2671854.7657	175.53	tb	tb
¢	707	505952.8756	2671950.2078	172.13	isl	isl
¢	708	505959.0215	2671867.8050	170.86	bb	bb
¢	709	505963.3718	2671941.9599	173.52	isl	isl
¢	710	505947.3938	2671879.4962	170.09	bc	bc
ф	711	505966.3480	2671934.0604	173.12	isl	isl
\$	712	505936.9483	2671891.6891	170.62	bc	bc
\$	713	505972.2455	2671930.1734	171.18	bb	bb
\$	714	505930.1152	2671905.0657	170.77	bc	bc
¢	715	505922.7397	2671915.4286	171.58	isl	isl
¢	716	505902.8359	2671963.4765	171.38	bw	bw
•	717	505919.4253	2671921.8475	173.16	isl	isl
•	718	505905.8056	2671958.6702	171.07	bc	bc
•	719	505914.1014	2671932.2193	172.63	isl	isl
•	720	505907.4574	2671956.7106	170.88	bc	bc
÷	721	505910 3316	2671942 7443	172.23	bc	bc
۰ ۵	722	505893 8409	2671883 7790	171.34	nier	pier
ф.	723	505912 5291	2671898 2761	170.26	pier	pier
å	724	505916 0080	2671897 7210	170.57	pier	pier
å	725	505915 1624	2671894 6906	171.50	pier	pier
~ &	726	505912 8451	2671871 3282	171.35	bo	hc
~ А	727	505909 4713	2671851 5925	171.03	bo	bo
~ А	728	505906 7026	2671832 7693	171.01	bo	bo
₩ ሔ	720	505500.7020	2071032.7033	171.0	nier	pier
₩ ሔ	720	505300.2003	2071014.0000	170.46	pier	pier
Ψ A	730	505003.0515	2071002.2301	170.40	inv	iov
ሞ ሔ	731	505913.2009	2071013.7370	173.00	inv	inv
ጥ ሔ	732	505020.0010	2071032.4132	101 CC	th	th
ሞ ሔ	733	505505.5170	2071000.3040	101.00	000	000
ም ሔ	734	505500.3000	20/1002.3/0/	104.00	eop	eop
Ψ A	730	505007.0002	2071700.0110	100.20	pier	pier
Ψ A	000	500307.0007	2071700.0241	100.12	pier 15	pier
Ψ A	001	500230.2107	2072044.0000	174.00	LL	LL
₩ A	000	506236.2376	2672044.5032	174.50	DD	DD
₩ A	802	506237.7267	26/2542./129	174.8/	tw .	[W
Ψ ^	003	506237.0413	2672341.6326	174.30	DW	DW
Ψ A	804	506229.9836	26/2042.7617	170.05	tw .	[W
ጭ ຼ	805	506229.2740	26/2542.6952	1/0.05	bw	bw
ጭ ຼ	806	506219.8511	26/2543.4689	169.27	bw	bw
œ ∽	807	506218.0563	26/24/3.3/14	166.14	bc	bc
÷	808	506210.0946	26/24/4.2460	164.28	bc	bc
÷	809	506191.8090	26/24/7.8990	165.89	bc	bc
<del>ب</del>	810	5061/9.2129	2672477.6856	166.31	bc	bc
•	811	506173.2047	2672477.6689	166.32	bc	bc
÷	812	506164.8102	2672478.0521	165.73	bc	bc
¢	813	506219.0126	2672546.3417	174.79	tq	tq
•	814	506153.1619	2672477.0259	168.15	bb	bb
¢	815	506219.8106	2672543.7550	174.79	tw	tw
¢	816	506220.7351	2672580.6408	171.65	tw	tw
¢	817	506220.1377	2672589.6407	164.88	bw	bw
¢	818	506218.7682	2672604.4570	162.65	bc	bc
¢	819	506223.5223	2672580.7560	172.33	tw	tw
¢	820	506238.3807	2672636.8764	170.50	tw	tw

Raw	Desc Mat	ching Point Groups	Include Exclude	Summary	List	
Nur	nber	Northing	Easting	Elevation	Raw Desc	Full Desc
¢	821	506223.1215	2672502.0846	167.48	bc	bc
¢	822	506219.9783	2672500.8613	165.13	bc	bc
¢	823	506209.6501	2672502.4968	165.14	bc	bc
¢	824	506193.6774	2672502.6335	165.22	bc	bc
¢	825	506193.6326	2672502.7137	165.20	bc	bc
¢	826	506265.1590	2672542.6927	180.46	еор	еор
¢	827	506176.1901	2672504.0212	165.57	bc	bc
¢	828	506281.3814	2672538.7337	180.80	еор	еор
•	829	506167.2476	2672504.4821	165.04	bc	bc
•	830	506275.6141	2672503.9485	180.65	еор	еор
	831	506262.0973	2672507.4142	180.50	еор	eop
	832	506251.9724	2672509.7718	179.76	tb	tb
•	833	506232.5126	2672513.3644	171.68	bb	bb
•	834	506230.6433	2672513.1774	169.95	eow	eow
	835	506270.1214	2672467.5024	180.29	еор	еор
	836	506255.2659	2672471.4931	180.14	еор	eop
•	837	506250.8540	2672473.6409	179.57	tb	tb
•	838	506224.7157	2672477.9707	172.27	bb	bb
•	839	506222.7747	2672478.9530	170.25	eow	eow
•	840	506220.0846	2672479.2891	170.12	bc	bc
•	841	506215.5697	26/2443.0368	169.67	bc	bc
•	842	506225.6421	26/2441.3633	1/1.83	bb	bb
•	843	506250.0644	26/2439.8156	1/9.89	tb	tb
•	844	506249.9266	26/2439./611	1/9.89	eop	eop
•	845	506246.6462	26/2440.8601	1/9.64	tb	tb
•	846	506215.5287	26/2415.924/	1/0.39	bb	bb
*	847	506264.3031	26/243/.3/21	180.04	eop	eop
*	848	506232.1139	26/2413.1/49	1/5.30	tb	tb
*	849	506239.3106	26/2411./259	1/9.36	tb	tb
Ŷ	850	506244.1818	26/2411.1631	1/9.65	еор	eop
₩ 	050	506212.4403	26/2400.7289	170.00	DC	DC
₩ 	052	506259.0382	2672409.3281	173.86	еор	еор
*	000	506213.6634	2072400.0174	170.72	DD	DD
*	004	506206.5014	20/2334.04/2	1/5./3	еор	еор
*	000	506231.6213	2072333.3220	170.10	1D 16	tb th
*	050	506241.0223	2072535.3373	173.00	iou	in.
*	859	506150 2667	2672303.0300	174.00	hh	bb
*	000 859	506135 1224	2672475.4100	191.53	th	th
*	860	506135.1224	2672471.3411	170.75	bb	bb
*	961	506132 //13	2672447.1330	193.62	th	th
*	862	506152.4415	2672440.4000	171 27	bb	bb
*	862	506134 2845	2672420.1044	1/1.2/	th	th
ф (ф	A38	506137 7994	2672396 5250	185.64	th	th
ф ф	865	506152 /287	2672400 3569	171 70	bb	bb
ф ф	220	506137.8669	2672396 / 57/	125.62	th	th
ф.	867	506153 8133	2672407 6582	167.89	hc	hc
ф (ф	868	506160 9/33	2672408 4042	165.9/	hc	bo
ф ф	630	506159 6500	2672430.4042	166 34	hc	bo
ф ф	870	506170 0058	2672433 9451	165.85	hc	bo
å	871	506152 8285	2672453 9262	169.09	hc	bo
а С	872	506168 1835	2672454 8994	166.72	hc	bo
ф ф	872	506184 9915	2672456 2007	166.40	hc	bo
	874	506198 4259	2672455 4409	165.94	hc	bo
w	0/4	500130.4233	2072403.4403	100.04	00	00

Raw Desc Mat	tching Point Groups	Include	Exclude	Summary	List	
Number	Northing	E	asting	Elevation	Raw Desc	Full Desc
875	506153.7970	267238	4.0219	166.46	bc	bc
876	506149.6465	267234	9.1567	164.98	bc	bc
877	506132.5627	267236	0.4920	184.81	tb	tb
878	506178.9928	267244	5.8250	165.74	bc	bc
879	506136.7272	267237	8.9741	187.65	tb	tb
880	506189.8183	267244	6.7654	165.70	bc	bc
881	506138.2425	267240	2.7467	184.64	tb	tb
882	506203.1111	267244	6.3792	165.32	bc	bc
883	506211.3444	267244	6.0028	166.85	bc	bc
884	506183.7246	267242	5.1702	165.52	bc	bc
885	506194.8722	267242	4.6919	165.54	bc	bc
886	506203.0208	267242	2.6750	164.90	bc	bc
887	506209.1806	267242	2.1987	167.20	bc	bc
888	506176.3691	267240	4.2722	164.71	bc	bc
889	506186.2811	267240	8.1865	165.12	bc	bc
890	506198.5768	267240	2.6546	167.18	bc	bc
891	506149.4716	267235	0.1375	165.67	bc	bc
1001	506266.6113	267254	2.8193	180.49	pk	pk
1003	506205.4782	267211	7.4550	182.91	pk	pk
1004	506223.2169	267254	8.7360	174.68	Start	Start
1006	506193.0323	267221	5.6794	176.96	pk	pk
1010	506266.6351	267254	2.7977	180.52	BS	BS
2001	506223.2169	267254	8.7359	328.08	oc1	oc1
2002	506266.6307	267254	2.8164	332.71	bschk	bschk
2003	506425.6200	267284	5.9526	349.60	archchk	archchk
3001	506184.0617	267248	0.9073	321.00	core1	core1
3002	506235.7657	267254	2.2303	320.58	core2	core2
3003	506163.2281	267233	4.9862	319.79	core3	core3
3004	506175.6110	267232	9.1752	319.64	core4	core4
3005	506148.2363	267226	7.7767	322.00	core5	core5
3006	506140.9126	267222	4.0445	322.39	core6	core6
3007	506179.4378	267249	2.4316	320.02	core7	core7
3008	506194.7078	267249	6.3329	319.71	core8	core8
3009	506178.5495	267250	6.7280	319.67	core9	core9
3010	506168.7827	267242	9.2698	319.79	core10	core10
3011	506123.6590	267228	7.7500	319.87	core11	core11

14. Appendix H: Topographic Map









16. Appendix J: Profile of Bushkill Creek Main Channel (North Side of the Island)



17. Appendix K: Profile of Bushkill Creek Secondary Channel (South Side of the Island)

REGISTRATION SEAL:							
E: (Hz & Vt) AS NOTED	DECEMBER 10, 2010		REVISION DESCRIPTION:	REVISED PER UPDATED SURVEY			
DRAWING SCALE	DATED:	REVISIONS:	NO: REVISED DATE:	01 03/06/2011			
BUSHKILL PROFILE	HYDROLOGY (CE-421)	DAVID BRANDES, Ph.D.	TEAM PROJECT	TEAM PROJECT	WTB	4 OF 5	NONE
TITLE:	COURSE:	PROJECT MANAGER:	PROJECT ENGINEER:	PROJECT SURVEYOR:	DRAFTSPERSON:	SHEET NUMBER:	COMMENTS:



18. Appendix L: Composite Plan View and Centerline Profiles of Bushkill Creek