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Civil and Environmental Engineering Services

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PROPOSED

LAFAYETTE COLLEGE

CEERC

Civil & Environmental Engineering Research Center

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Report 6

**Hummel Building - Structural Design
Report**

Site

Former Hummel Lumber Supply at 900 Bushkill Drive

City of Easton, Northampton County, Pennsylvania

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I Design Loads

I.1 Dead Loads

	<u>Unit weight</u>
1. Existing Wood Deck	12.5 psf
2. Beams	VARIED
3. Joists	VARIED
4. Columns	VARIED

I.2 Live Loads

	<u>Uniform</u>
1. Variable Use Office Space*	100 psf
2. Light Manufacturing	125 psf

*100 psf live load was chosen to conservatively estimate that any portion of the floor may be corridor.

I.3 Roof Loads

	<u>Dead</u>	<u>Live</u>	<u>Snow</u>
1. Edge Column	66.25 k	32 k	7.36 k
2. Corner Column	33.12 k	16 k	3.68 k

II Retrofit Design

II.1 Structure Lab Beam Retrofit Design – 40 ft Span

Beam 5 – typical

Tributary width	8 ft
W_u , uniform floor load	1.4 klf
P_u , point loads from columns above	19.6 kips
M_u (excluding self weight of reinforcement)	515.2 kip-ft
$M_u/2$ (1 beam on either side of existing wood)	257.6 kip-ft

From Table 3-2 in AISC Manual 2013 Edition
W16x40

$$\Phi_b M_n = 274 \text{ kip-ft}$$

Check selfweight – Corrected M_u

$$265.6 \text{ kip-ft}$$

Alternative Beam Design

Use prefabricated steel joists to reduce tributary width to interior beams and columns on floors 1 and 2.

Beam:	
Tributary Width	4 ft
W_u , uniform floor load	0.7 klf
P_u , point loads from columns above	9.8 kips
M_u (excluding self weight of reinforcement)	257.6 kip-ft
$M_u/2$ (1 beam on either side of existing wood)	128.8 kip-ft
From Table 3-2 in AISC Manual 2013 Edition W12x26	$\Phi_b M_n = 140$ kip-ft
Check selfweight – Corrected M_u	133.8 kip-ft
Joist	
Tributary Width	2 ft
W_u , uniform floor load	0.35 klf
From New Millennium Joist Tables 22K5 Joists at 2 ft center to center spacing	

II.2 Typical 2 Bay Beam Reinforcement – 28 ft Span

Beam 5 – typical

Tributary width	8 ft
W_u , uniform floor load	1.4 klf
P_u , point loads from columns above	19.6 kips
M_u (excluding self weight of reinforcement)	271.6 kip-ft
$M_u/2$ (1 beam on either side of existing wood)	135.8 kip-ft
From Table 3-2 in AISC Manual 2013 Edition W12x26	$\Phi_b M_n = 140$ kip-ft
Check selfweight – Corrected M_u	138.4 kip-ft

II.3 Column Reinforcement

Parimeter Columns – A2,A3,A4,A6,A5,A7,D10,D12,D13

Tributary Area	123.68 ft. ²
Floor Height	10ft.
P_u	184.87 kips
From Euler buckling analysis 2C6 x 10.5	$\Phi P_n = 223.15$ kips

Perimeter Columns A8,A10,A12,D8

Tributary Area	48.8 ft. ²
Floor Height	10ft.
P _u	151.46 kips
From Euler buckling analysis	
2C6 x 8.2	ΦP _n = 177.47 kips

Perimeter Columns D4 –D7

Tributary Area	48.8 ft. ²
Floor Height	10ft.
P _u	174.52 kips
From Euler buckling analysis	
2C6 x 8.2	ΦP _n = 177.47 kips

Perimeter Columns B1,B14,C1,C14

Tributary Area	102 ft. ²
Floor Height	10 ft.
P _u	170.08 kips
From Euler buckling analysis	
2C6 x 8.2	ΦP _n = 177.47 kips

Corner Columns A1,A14,D14

Tributary Area	24.4 ft. ²
Floor Height	10ft.
P _u	82.57 kips
From Euler buckling analysis	
2C6 x 8.2	ΦP _n = 177.47 kips

Interior Columns – B10,B12,B13

Tributary Area	173 ft. ²
Floor Height	10ft.
P _u	67.76 kips
From Euler buckling analysis	
2C6 x 8.2	ΦP _n = 177.47 kips

II.4 Loading Bay – New Steel Design

Loading

Dead Load	50 psf
Live Load (Light Manufacturing)	125 psf

Typical Beam

Tributary width	8 ft
W_u , uniform floor load	2.08 klf
M_u (including self weight)	204 kip-ft

From Table 3-2 in AISC Manual 2013 Edition W12x26	$\Phi_b M_n = 223 \text{ kip-ft}$
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Increased capacity of this beam due to composite action

Typical Column

Controlling Tributary Area	140.82 ft. ²
Floor Height	10 ft.
P_u	36.61 kips

From Table 4-1 in AISC Manual 2013 Edition W8x31	$\Phi_c P_n = 317 \text{ kip-ft}$
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Bending from an asymmetric tributary area was not analyzed, due to the allowable load being 8 times the applied, this can be assumed as being adequate

Steel Decking with Concrete Slab

Clear Span (2 bays)	7.5 ft.
From VULCRAFT manual 1.5 VLR 22	Slab thickness- 3.5 in.
Shear Studs	$\frac{3}{4}$ in. studs 1ft. C-C

II.5 Foundation Recommendation

Soil conditions and existing foundations are unknown, so calculations could not been done. Due to the largely increased loads due to the green roof, more investigation of the foundation system of the building should been done to confirm that it is adequate for the loads. Recommendations for investigate are addition of concrete pilasters or indermediate foundation system.

II.6 Existing Wood Column/Beam Analysis

Analysis of the adequacy of the existing wood column and beam structure was not completed due to lack of information on the type of wood and inexperience with wood design/analysis. Due to the increased loads on the structure, this analysis should be completed before final approval of the design. The structural plans do not include all features of the building, such as stair wells. These should be included and analyzed before final approval of the design.

II.7 Design Summary

The retrofit design included the reinforcement of beams, that instead of spanning only 12ft. or 16ft. were increased to 28 and 40ft. spans. The loads used for this design were a live load of 100 psf (variable use office space) and a variable dead load. The beams spanning 28ft. included reinforcing the existing wood beam with two I-beams (See Figure II.1). For the beams spanning 40ft. in the structural lab, the retrofit also included reinforcing the existing wood beam with two I-beams and the addition of 22K5 joists spaced at 2 ft. center to center.

Due to the increased loads from both the green roof and increased tributary areas of the column, reinforcement was required. The loads used for this design were a live load of 100 psf (variable use office space) and a variable dead load. The design included reinforcing the existing wood columns with two steel C-Channels. The two sizes of C-Channels used were C6x8.2 and C6x10.5. See Figure II.2 for a detail of this reinforcement and Figure II.3 for detail of the connection of the reinforced beams and columns.

The design of the loading bay included the design of new steel columns and beams and steel decking with a concrete slab. See Figure II.4 for the plan view of the loading bay. The loads used for this design were a live load of 125 psf (light manufacturing) and a dead load of 50 psf. A W8x31 was found to be adequate for the columns and W12x26 was adequate for the beams. The thickness of the deck using the VULCRAFT manual was 3.5 inches and the adequate size and spacing of shear studs are $\frac{3}{4}$ " studs at 1 ft. center to center spacing.

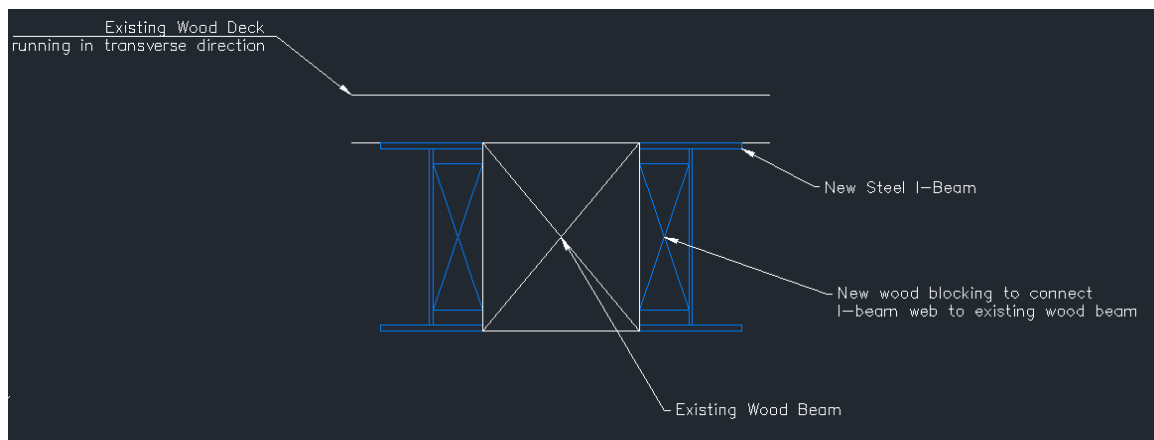


Figure II. 1: Detail of Beam Reinforcement

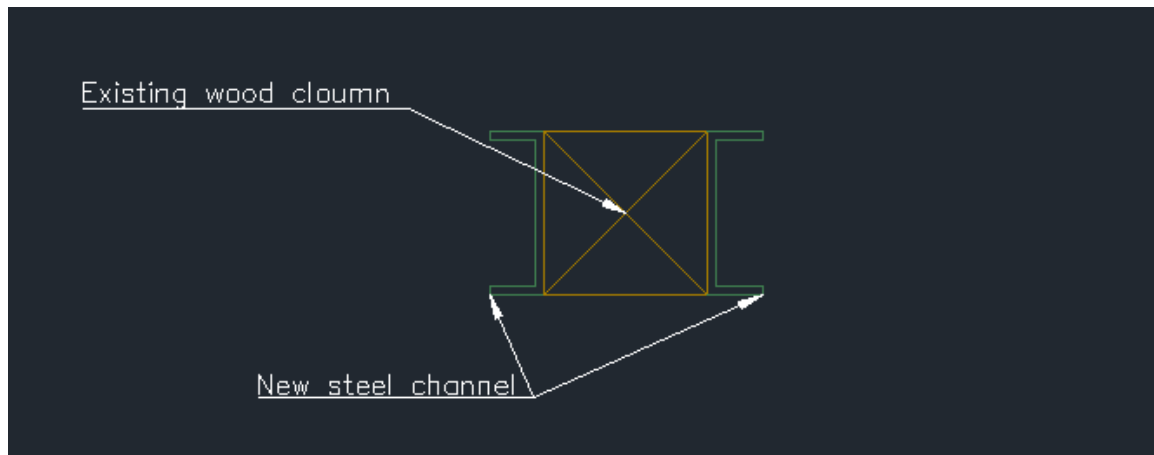


Figure II. 2: Detail of Column Reinforcement

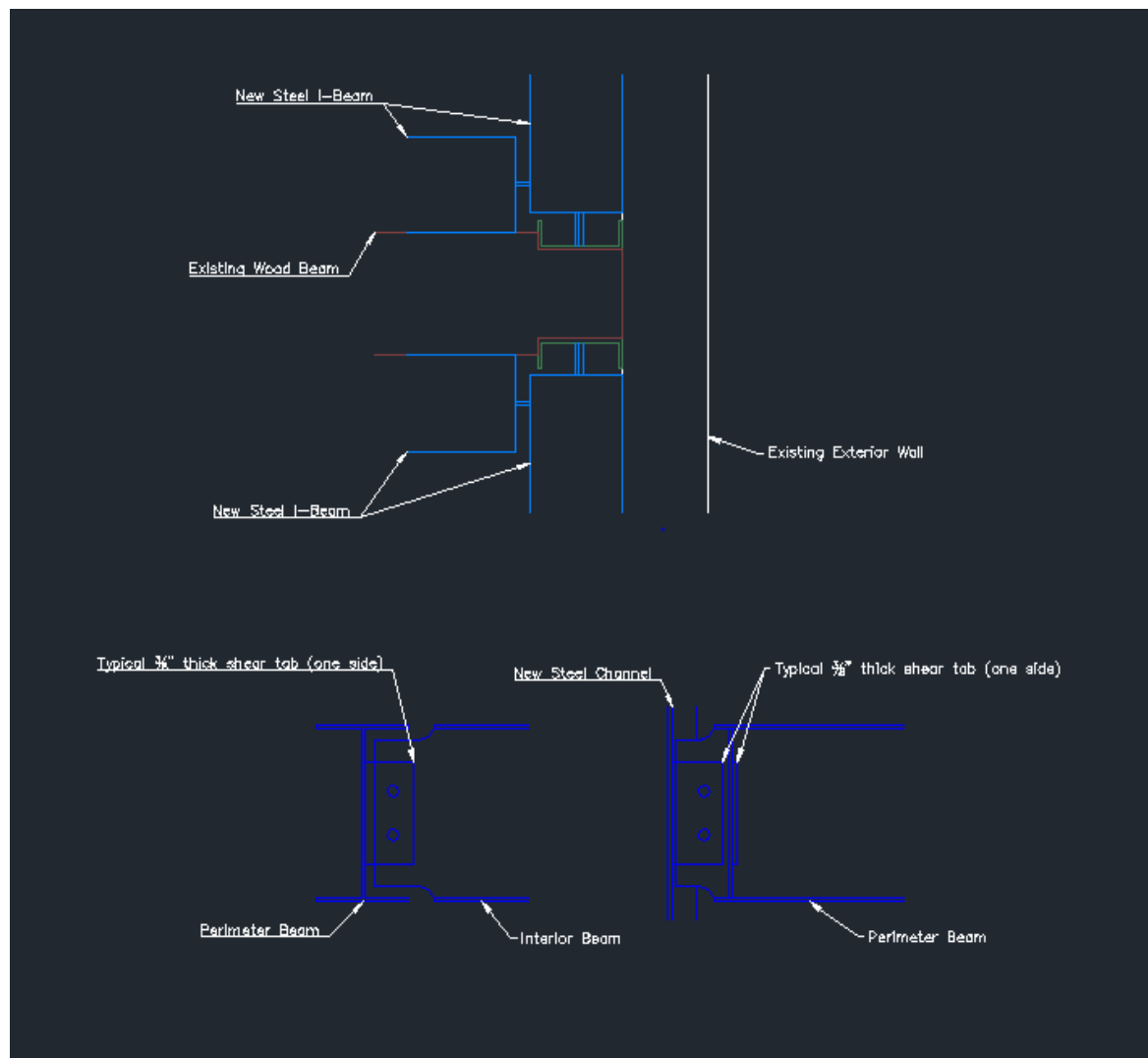


Figure II. 3: Detail of Reinforced Beam to Column Connection

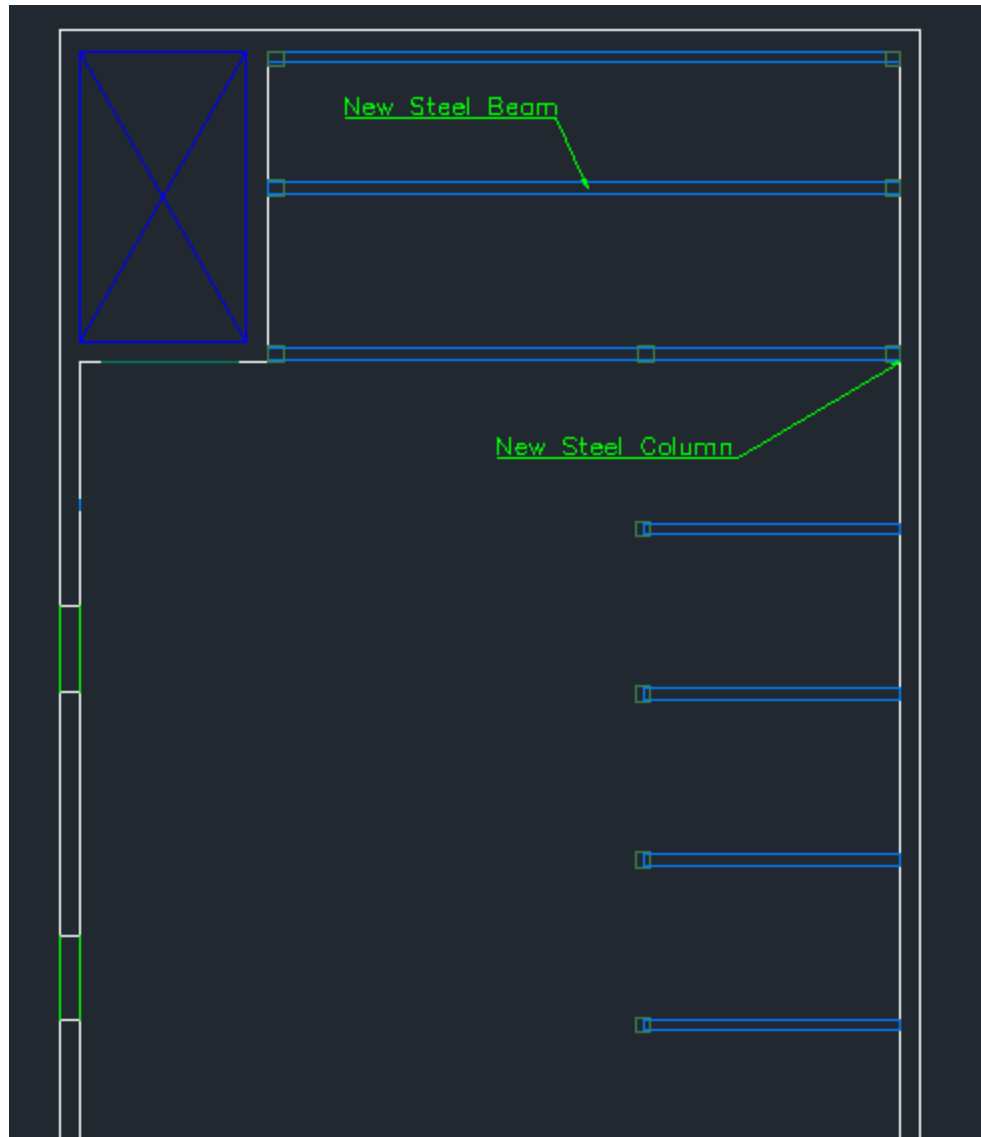


Figure II. 4: Plan View of Loading Bay